

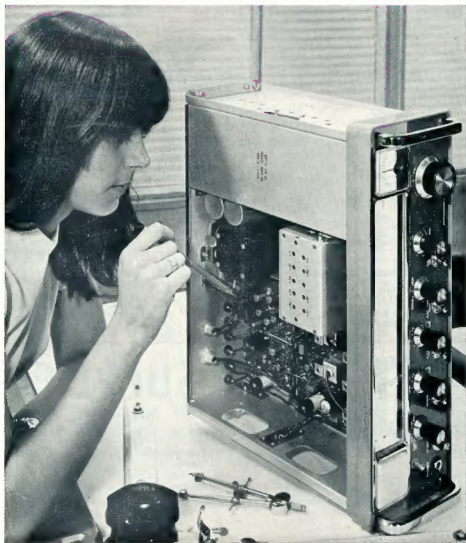
# amateur radio

VOL. 100 No. 6

JUNE, 1971

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# amateur radio

JOURNAL OF THE WIRELESS INSTITUTE OF AUSTRALIA. FOUNDED 1910



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## CONTENTS

### Technical Articles:—

	Page
A Solid State F.M. Transceiver—Some After-Thoughts .....	9
Australia Balloon Flights—A Preliminary Report .....	17
Home Station Antenna for 160 Metres—Part Two: Vertical Polarised Antennas .....	3
The Class C Radio Frequency Amplifier—Lecture No. 13 .....	10

### General:—

Announcing a Special Call and Prefix .....	18
Australian 2 Metre F.M. Repeater Directory .....	13
Cook Bi-Centenary Award .....	28
Correspondence .....	7
"CQ" Awards .....	28
DX .....	25
Federal Comment: Novice Licensing—Again .....	2
I.A.R.U. Region 3 Association Conference, Tokyo, 1971 .....	21
Key Section .....	18
May I Talk to You About the 35th Federal Convention in Brisbane .....	19
New Call Signs .....	13
Norfolk Island DX-pedition .....	28
Overseas Magazine Review .....	26
Prediction Charts for June 1971 .....	16
VHF .....	23
W.I.A. D.X.C.C. ....	11
W.I.A. V.H.F.C.C. ....	28
W.I.A. 52 MHz. W.A.S. Award ..	26

### Contests:—

VK-ZL-Oceania DX Contest, 1970 Results .....	14
VK2 Mid-Winter V.H.F.-U.H.F. Contest .....	22

### COVER STORY

The Eddystone model EC990S is a modern fully transistorised UHF receiver for AM/FM operation in the range 230-870 MHz. Designed for fixed or mobile operation, this unit has applications in meteorological service, radio astronomy, aerial investigation and in radio laboratories. In addition to audio and video outputs, a low impedance output at the i.f. of 38.5 MHz. is provided to drive ancillary equipment. Further information is available from R. H. Cunningham Pty. Ltd.

## NOVICE LICENSING - AGAIN

The Federal Council at the 1970 Federal Convention divided equally on the question of whether or not the Wireless Institute of Australia should press for the introduction of some form of Novice licence in Australia. The Federal Council did, however, direct that the Federal Executive seek further information to be embodied in a report so that the question could be considered further. The Federal Executive sought the assistance of the New South Wales Division and accordingly a committee of that Division, under the chairmanship of Mr. Rex Black, VK-2YA, was formed. The report of the committee was received by the Federal Executive on 1st April, 1971, copied and posted to all Federal Councillors on 2nd April—that is exactly one week before the Federal Council met in Brisbane for the 1971 Federal Convention. The report has received universal praise; indeed the Federal Council formally recorded its deep appreciation of the work of the committee.

Yet, the Federal Council decided to defer decision on the matter. I know that very many people were interested in this question. Perhaps some will regret the decision to make no decision at this time. Perhaps it could be seen by a few as evidence of a thoroughly negative attitude. To draw such inference, however, to be less than fair. First, let us look at the report. It raises, I believe, all the issues relevant to Novice licensing clearly and succinctly. In requesting such a report, the Federal Council was seeking as much factual evidence as possible upon which a decision could be based. The report provides this information. I have found this report most helpful on one of the most complex and difficult topics that have been considered in recent years.

In brief, the report recommends that the W.I.A. should seek the introduction of a "Novice" type of licence in Australia. This is necessarily a value judgment. There is no single fact that points unequivocally one way or the other. For example, the two countries with the highest ratio of Amateurs per head of population in the world are the United States of America and New Zealand. One has—the other does not have—Novice licensees.

The report suggested, for discussion, that a Novice licence should be sought on the following basis:

1. A lower standard theory examination than that required for A.O.C.P. and A.O.L.C.P.

2. The same standard regulation examination as is required for the A.O.C.P.-A.O.L.C.P.
3. A five words per minute Morse test.
4. That the Novice licensee will use:
  - (a) A crystal controlled transmitter.
  - (b) Not more than 10 watts d.c. input.
  - (c) C.w. only.
5. The same age limit would be imposed as is imposed for A.O.C.P. and A.O.L.C.P.
6. A limited term licence only would be issued.
7. The licence would take with it the right to operate fixed, mobile or portable.
8. Special call signs would be allocated to Novice licensees.
9. A character reference would be required before a Novice licence is issued.
10. The Novice licensee would be permitted to operate on the following bands:—

1800 - 1860 KHz.  
3505 - 3525 KHz.  
7010 - 7050 KHz.  
21030 - 21150 KHz.  
28040 - 28200 KHz.

In addition, a number of other proposals were suggested. I have no doubt that this report will provoke spirited discussion. **That is exactly what it should do.** The report is printed as Appendix E to the Minutes of the Federal Convention. Your Federal Councillor has a number of copies. Please approach him for further details and please discuss the matter and express your view to your Federal Councillor and Divisional Councillors.

At the outset, I stressed the date the report was received by the Executive and circulated to the Federal Councillors. The committee, under Mr. Black, was appointed towards the end of 1970. It sought the views of many people and engaged in a volume of correspondence described by one Federal Councillor as "fantastic". That the committee achieved its object of producing a report prior to the Federal Convention is no mean feat. Perhaps, however, it is reasonable to ask whether the fact that a decision was deferred means that this effort was wasted. Emphatically, no. Formally, and particularly informally, the Federal Council engaged in a spirited and very deep discussion of the many issues involved. Had that report not been received in time for the Convention one of the most

useful discussions that have taken place in recent years would just not have occurred.

The introduction of a Novice licence system raises many issues fundamental to our hobby—the very purpose of the Amateur Service, the relationship of one type of licence with another, the virtues of quality as against the virtues of quantity are all relevant. Then, what do we set out to achieve with a Novice licence? How do we best do it? Do we take any different view of the two types of licence we already have? These are all equally relevant questions before we finally decide—if we do—to seek a Novice type licence and, even if we do so decide, the conditions of issue of such a licence raise question after question. No, the deferring of a decision was not evidence of negative thinking—rather it was a tribute to a magnificent report that deserves the fullest consideration and appreciation of the depth of a problem that, whilst in the past has been contentious, has not before been considered so completely. The deferring of the decision also gives each member the opportunity to re-consider his views and to take part in the formulation of one aspect of the Institute's policy that will undoubtedly and fundamentally affect our hobby for the future—whichever way the decision goes.

Finally, the matter does not have to wait another year. Your Federal Councillors are in regular communication with one another and with the Federal Executive. A decision can be made prior to the next Federal Convention if it appears that the pendulum previously finely balanced between "for" and "against" moves clearly in one direction or the other, thus answering the question "whether". If the answer is "for" then the question "what?" (an equally complex question) must be answered. I believe, too, that given a consensus, that question, should it arise, can also be answered prior to the next Convention.

Mr. Black and his committee have made the way open for our organisation to make an informed decision on a topic that has troubled many people. A snap judgment would have pleased some, displeased others, depending which way it went. A considered judgment will, whichever way it goes, justify the enormous amount of work of the committee. This is a question that must fundamentally affect the future of our hobby. Please make sure that your voice is heard.

—MICHAEL J. OWEN, VK1KI,  
Federal President, W.I.A.

# HOME STATION ANTENNA FOR 160 METRES

## Part Two—Vertical Polarised Antennas

J. A. ADCOCK,\* M.J.E. (Aust.) VK3ACA

### GENERAL

The basic medium frequency antennas are the quarter wave vertical (or Marconi) and the half wave vertical. An antenna having a better radiation in the horizontal direction is the five-eighth wave vertical, this behaves like half an extended double zepp. Both quarter wave and half wave verticals present a pure resistance load at the base. The quarter wave has a definite resistance of about 40 ohms which can be obtained from the formula. The half wave has a high resistance feed point at the ground. An antenna length other than a quarter wave or half wave has some reactive and some resistive component. The equivalent circuits of the loads of these antennas are shown in Fig. 3. In this article we are mainly considering antennas with a pole or leg length of less than a quarter wave and only verticals which are base fed against ground.

The quarter wave antenna when fed in series with the ground will be resistive only. For a short antenna the load can be looked on as a capacitance in series with a resistance. As the antenna is shortened the resistance will become smaller and the capacitive reactance will become larger (smaller capacitance). Because the effective series reactance becomes higher, the load requires a higher driving voltage, this voltage being largely out of phase with the current. In other words the load has a poor power factor.

This effective series reactance can be tuned with a variable series inductance,

and when this is done the resistance of the load is presented to the transmitter, the value of which is equal to the radiation resistance plus the loss resistance. For a short antenna the radiation resistance reduces with the square of the length of the antenna.

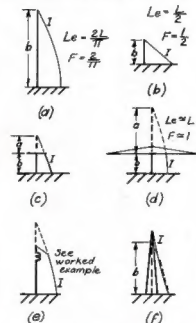


Fig. 4.—Showing the current distribution on some vertical antennas. (a) and (b) are used in the text to indicate electrical lengths of the component parts.  $l$  is the actual length of the radiating section. The effective length and the "form factor" are shown for some cases.

In some circumstances it may be desirable to consider the load as an equivalent parallel circuit as shown in Fig. 3. For a short antenna the equivalent parallel circuit will be one with a very high resistance and a high capacitive reactance. The equivalent series circuit is the one most commonly used. The conversion formula for parallel to series circuits is not given to avoid unnecessary complication. It is necessary to know the reactance to make the calculation. Series parallel conversion and reactance have been introduced later with references as an incidental.

As the antenna is made longer and approaches a quarter wave, the series reactance approaches zero or the parallel reactance approaches infinity, and the resistance in both cases approaches 40 ohms. As the antenna is lengthened beyond a quarter wave the series reactance increases and the series reactance becomes inductive. The series inductive reactance again approaches zero as the antenna length approaches a half wave and the resistance becomes a high value.

The distribution of current on a vertical antenna is shown in Fig. 4. The effective lengths of the antenna for the purpose of approximate calculation are also shown. Fig. 4a shows the current distribution for a quarter wave antenna, the distribution being approximately sinusoidal (Ref. 3). Fig. 4b shows the position for a short vertical. It will be noted that this distribution is approximately "triangular".

As pointed out already, a short antenna will necessarily have a low feed point resistance and therefore a large current. The driving voltage will also be high due to the high series reactance. An equivalent series circuit of a complete tuned short antenna is shown in Fig. 5. The constants are considered lumped. From the circuit it is obvious that if the losses are to be minimal the radiation resistance should be high and steps should be taken to reduce losses. In the antenna in Fig. 4b the current will be maximum at the bottom and zero at the top. As a result, current at the feed point is twice the average current and therefore the radiation resistance is low, also a large base loading inductance is required to tune the antenna.

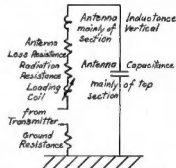


Fig. 5.—Showing a series equivalent circuit of the whole antenna. The main parts are shown lumped.

A much better distribution of current is achieved by "top loading", shown in Figs. 4c, d, and e. The top load can be made large enough so that the current in the vertical section is practically constant over the length considered. In fact the top can be made large enough so that the antenna will resonate.

Large capacitive top loading has the following advantages:

1. The current distribution in the radiating section is optimum, resulting in maximum radiation resistance.
2. Minimum tuning inductance is required.
3. The large capacitive top ensures minimum voltage stress to produce the necessary electrostatic field, hence minimum tendency to corona.

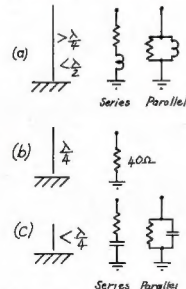


Fig. 3.—Showing the antenna together with the equivalent series and parallel circuit of the load when the antenna is fed in series with the ground.

\* P.O. Box 106, Preston, Vic., 3072.

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Initially in this discussion the top is considered to be symmetrical and therefore would radiate very little since currents flow in opposite directions and produce a largely cancelled field.

A symmetrical antenna with a straight wire top is very ancient and goes under the name of "T". The top load, however, can take several other forms, e.g. an umbrella, several horizontal radials, a flat disk, an inductively loaded whip, a cylinder or a sphere. An antenna with a single top wire at right angles is known as an "inverted L". A "sloping antenna" is also a vertical and these will be dealt with in a separate section.

The top loading will have an effect on the antenna like an extra length of wire vertically (non-radiating). This equivalent effective vertical is shown as length "a" in Figs. 4c, d and e, and the vertical radiating section is shown as length "b". The current distribution over the real and virtual part of the antenna in all cases except Fig. 4f is close to sinusoidal (Ref. 3). The shortening effect of a tapering antenna is only illustrated here and is not analysed.

## CALCULATIONS FOR VERTICAL ANTENNAS

Radiation resistance of a vertical antenna when fed in series with the ground is given by—

$$R_s = \frac{1580 L_s^2}{\lambda^3} \dots \dots (1)$$

where  $L_s$  = the effective length of the antenna.

$\lambda$  = wavelength.

Fre- quency	$\lambda$ metres	$\lambda$ feet	$\lambda/4$ feet
1.8	166.7	546.8	136.7
1.825	164.4	539.3	134.8
1.85	162.2	532.0	133.0

Since we are considering the vertical component only any horizontal radiation resistance can be considered part of the loss. This value is usually small. In the graphs given here the electrical length of the antenna is taken as  $\lambda/4 = 1$ . This was considered to be simpler for calculation than  $\lambda/4 = 90^\circ$ . If calculations are made from tables, angular lengths would have to be used. In the examples given here no reference is made to velocity factor or end effect as these values should make a small difference only.

The effective length of the antenna and the form factor of the current distribution are as defined earlier.

$$F = L_s + L$$

$$L_s = F \times L \dots \dots (2)$$

where  $F$  = form factor.

$L$  = actual length over which the current distribution is being considered.

The vertical component of the antenna, the length over which the vertical current distribution is considered, is usually the gap between the top load and the ground.

Also—

$$F = \frac{\text{Average Current}}{\text{Base Current}} \dots (3)$$

$$\text{Average Current} = \frac{\text{Area under Current Distribution Graph}}{L} \dots (4)$$

In the case of a triangular distribution of current (Fig. 4b), the average current must be half that of the base current. Therefore it would radiate the same power as a wire of half the length carrying a constant current equal to the base current ( $F = \frac{1}{2}$ ). In the case of Fig. 4d, the effective length is equal to the actual length ( $F = 1$ ).

The form factor for a quarter wave is  $2 \div \pi$ , as shown in Fig. 4a. The true form factor for a radiating section of wire is given below.

From equations 3 and 4:

$$F = \frac{\int_{x=0}^{x=L} i \, dx}{L \cdot i}$$

where  $i$  = current at distance  $x$  from the end of the antenna.

$L$  = length of the radiating section being considered.

$i$  = base current.

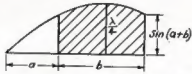


Fig. 6.—Illustrates the method used for equation 5.

Consider Fig. 6. The length "a" is the equivalent electrical length of the top (not necessarily the actual length) and length "b" is the electrical length of the radiating section. The current distribution in the wire is sinusoidal. From the equation the electrical length  $L$  must be taken in radians and equals length "b".

$$F = \frac{\int_{x=a}^{x=b} \sin x \, dx}{\text{radian } b \times \sin(a+b)} = \frac{\cos a - \cos(a+b)}{\text{radian } b \times \sin(a+b)} \dots \dots (5)$$

$a$  and  $b$  can be taken as the angular length  $\lambda/4 = 90^\circ$  and the figures taken

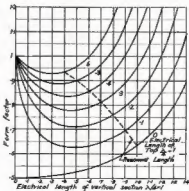


Fig. 7.—Curves of "form factor" against electrical length of the radiating section for various lengths of top load.

from tables. Note that if  $(a + b)$  is greater than  $90^\circ$

$$\cos(a + b) = -\cos[180 - (a + b)]$$

Calculations from equation 5 are shown plotted in Fig. 7, and using equation 6 below, Fig. 8 was plotted.

Taking:

$$\text{electrical length} = L \div \lambda/4$$

and from equations 1 and 2

$$R_s = 98.75 (\text{elect. length} \times F)^2 \dots (6)$$

Example for a simple quarter wave vertical:

$$R_s = 98.75 \times (1 \times 0.636)^2 = 39.9$$

It must be pointed out that this method of calculating radiation resistance is a simplified method and is only correct if the radiating section of the antenna is short. If it is near a quarter wavelength or longer the radiation resistance will be less by a small amount, however the results given by the formulae and graphs shown here should be sufficiently accurate within the range shown.

According to the formula, as the antenna approaches a half wavelength the radiation resistance approaches infinity. This is obviously erroneous. If the total electrical length of the antenna is more than 1.4 of a leg length of a quarter wave, the formulae should not be used. The radiation resistance at the base of a half wave vertical cannot be accurately calculated but would be in the order of several thousand ohms.

A choice of methods for determining the form factor of the current distribution on an antenna has been given and these are summarised as follows:

1. If the current distribution conforms nearly to the standard forms shown in Fig. 4, these may be applied.  $F$  for a short vertical = 0.5 and  $F$  for a heavily loaded vertical = 1, the latter may not be sufficiently accurate on 160 metres.
2. If the current distribution curve is known, equations 3 and 4 can be applied and the areas under the current curve determined graphically or by measurement.
3. By application of the graphs of equation 5.

## Effective Electrical Length of Top Load

This matter created some discussion as some authorities state that in the case of a "T" the effective length is equal to half the length of the top, that is, the "inverted L" section only and other authorities seem to leave the matter open.

The following would appear to be correct (Ref. 4):

1. With an "inverted L" the effective electrical length of the top is equal to the actual electrical length.
2. The electrical distance of the point being considered on the antenna from the current or voltage point (virtual or otherwise) is dependent upon the reactance component at that point.
3. The antenna can be considered as a wire with approximately 600 ohms characteristic impedance.

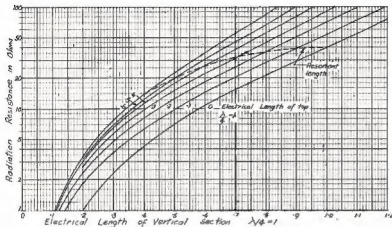


Fig. 8.—Radiation resistance of a vertical against height for various equivalent lengths of top load.

### Worked Example

A "T" antenna is 45 feet high and has a 66 ft. flat top. With 100 watts input to the final the antenna current is 1.8 amps.

Electrical length of half top  
 $(\lambda/4 = 1) \dots \dots \dots = 0.245$   
 Equivalent electrical length  
 of top (Fig. 10)  $\dots \dots \dots = 0.43$   
 Electrical length of vertical  
 section  $\dots \dots \dots = 0.332$   
 Form factor (Fig. 7)  $\dots \dots \dots = 0.86$

From equation 6

$$R_a = 98.75 \times (0.86 \times 0.332)^2 \\ = 8.0 \text{ ohms.}$$

From equation 7

$$R = \frac{100 \times 0.7}{1.8^2} \\ = 21.2$$

Efficiency of antenna  $= 8 \div 21.2$   
 $= 0.38 \text{ or } 38\%$

$$R_L = 21.2 - 8.0 \\ = 13.2 \text{ ohms}$$

probably mainly ground resistance.

### THE CENTRE LOADED VERTICAL

The effect of an inductance in a vertical is to increase the capacitance loading of the top from the point of view of the bottom, Fig. 8e. In other words, the top is made to look larger. The top carries maximum voltage to provide the electrostatic field whereas the bottom section carries maximum current to provide the magnetic field. As well as a top whip the loading coil can be placed below any other form of top of small dimension.

The method has its main application where space is limited and the top is small. It is not as satisfactory as a large capacitive top load. While it does make the current and voltage distribution on the antenna more satisfactory (resulting in a higher radiation resistance), it does add extra losses into the circuit. The tendency to corona is increased.

The inductance of the coil will be much greater to tune the antenna to resonance at the centre than at the base and therefore the coil will be more lossy. Care should be taken not to tune the antenna over resonance or the coil may become very lossy. The best compromise is some centre loading and some base loading. Modern practice appears to be to keep the centre loading coil long and thin to reduce common mode radiation loss. For idealised cases of current distribution, the radiation resistance can be calculated from equations 3, 4 and 6.

The centre loaded whip as well as the helical whip have their main application to portable and mobile, but these applications are not discussed here.

### Worked Example

**Example 1.**—A centre loaded whip has a total height of 35 ft. The distance from the base to the coil is 25 ft. and from the coil to the tip of the whip is 10 ft. Current was measured at the base of the antenna as 1.5 amps. and at the junction between the lower part

Power input to the antenna  $= I'R$   
 $R$  = the total resistance of the load  
 $R = R_a + R_L$

Since  $R$  is an unknown quantity  
 $R = W \div I'^2 \dots \dots \dots (7)$   
 $W$  = power input to antenna.

The power input to the antenna can be estimated from the final input. For a class C amplifier, 70% efficiency is reasonable. For a sideband rig, the manual should give sufficient information to estimate the power output.

$$\text{Radiation efficiency of antenna} \\ = \frac{\text{power radiated}}{\text{power input to antenna}} \\ = \frac{I^2 R_a}{I'^2 R} \\ = \frac{R_a}{R} (\times 100\%) \dots \dots \dots (8)$$

$R_a$  is found from graphs or calculation and  $R$  is found from equation 7. It is possible to use a Q meter or a bridge to obtain the load resistance but these were found to have certain difficulties as referred to in the discussion. The r.f. ammeter should be of the thermocouple type and should be checked against an ammeter at 50 Hz. It may be useful to obtain the loss resistance.

$R_L = R - R_a \dots \dots \dots (9)$   
 In a grounded vertical antenna,  $R_L$  will be mainly ground resistance.

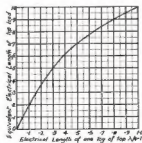


Fig. 10.—The length of one leg of the top of a T is plotted against the length of a single wire which would have the same effect.

4. The no-load reactance curve for an unloaded 600 ohm line is near enough to correct except close to the voltage loop.

5. At the junction of the "T" the reactance load of each half will add in parallel to produce a reactance of half that of the individual line.

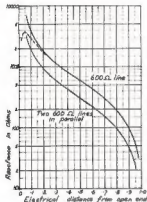


Fig. 9.—Curves for the open circuit capacitive reactance of a 600 ohm line or antenna. The lower curve represents the reactance when two lines are joined in parallel, such as the junction at the top of a "T" antenna. The short dotted curve at the top left shows the deviation in effective series reactance when the line is loaded with an s.w.r. of 12. For higher s.w.r.'s the deviation would be even less.

Fig. 9 has been drawn based on wire and two wires in parallel. (The mutual capacitance and inductance between the wires was not taken into account.) From these graphs, Fig. 10 was plotted to determine the equivalent electrical length of two lengths of wire (a "T" top).

### Efficiency of Antenna

The radiation resistance of the antenna is dependent mainly upon the configuration and not on the loss resistance. The actual resistance of the load of the antenna will equal the radiation resistance  $R_a$  plus the loss resistance  $R_L$ .

Power radiated  $= I'R_a$

$I$  = the current at the feed point.



and the coil as 1.0 amp. What is the radiation resistance?

From equations 3 and 4

$$F = \frac{(1 + 1.5)}{2} \times 25 + \frac{1 \times 10}{2} \\ = 0.69$$

Total electrical height = 0.259.

From equation 6

$$R_a = 98.75 (0.259 \times 0.69)^2 \\ = 3.17 \text{ ohms.}$$

In the above the current distribution curves were taken as straight lines. If you don't believe that the ammeter can be inserted between the vertical section and the coil, then consider this problem.

**Example 2.**—In the antenna in Example 1, it was found impossible to insert the ammeter two-thirds of the way up, but it was observed that 38 micro-henries were required at the base to bring the antenna to resonance. What is the radiation resistance? (Solution at some future date if requested.)

## METHODS OF FEEDING

When the antenna is series fed, methods of tuning the antenna depend upon the type of load expected. For efficiency it is desirable to use the minimum tuning circuit possible and this is usually a single variable inductance in series with the antenna capacitance. When the antenna is tuned by a series circuit the effective series resistance of the antenna will be presented as a load to the transmitter.

Circuit Fig. 11a is used where the antenna is shorter than a quarter wavelength. Since a short antenna has a low resistance, the tuning circuit of the transmitter must be adequate to handle this. The coupling capacitor of the pi of the final tuning should be large to prevent overcoupling between the two tuned circuits. Overcoupling could result in harmonic radiation and makes tuning difficult. Circuit Fig. 11c is used where the antenna is over resonant—effectively more than a quarter wavelength. Where the antenna is close

to resonant it may be either slightly inductive or capacitive. If the antenna is slightly capacitive, this is simply tuned by only a few turns of inductance, but if the load is slightly inductive a small capacitive reactance is required and hence a very large capacitor. The circuit of Fig. 11b is probably the best to use here. Also, circuit Fig. 11b may be used where no variable inductance is available.

Figs. 11d and 11e are parallel tuned circuits in which the antenna load is effectively in parallel with the tuned circuit. To understand this it is best to consider the effective parallel circuit of the load, Fig. 3. Here the effective parallel resistance is high and the coil behaves as a matching transformer. (It should be realized that there are several ways of looking at these circuits and whether you consider it as a circuit with low series resistance or with a high parallel resistance is a matter of convenience.)

These circuits are particularly applicable where the antenna tuning unit is remote from the transmitter and/or where it is necessary to match into a line. Other arrangements such as pi coupling may also be applicable.

Shunt feeding the lower end of the antenna has some application where the antenna is permanently connected to the ground, Fig. 11f. The antenna is fed with something like a gamma or a half delta match. It is suggested that this method, while satisfactory with a near resonant antenna, could be difficult with a shortened antenna. Large circulating currents would be present in the closed loop of a non resonant antenna which would reduce efficiency and make tuning difficult.

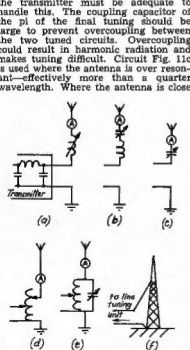


Fig. 11.—Illustrating various methods of feeding and tuning.

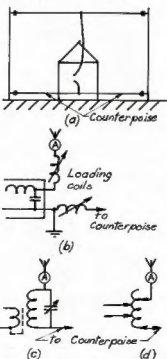


Fig. 12.—Methods of tuning a counterpoise.

## EARTHING AND COUNTERPOISING

The most lossy part of a short vertical antenna is the ground. Ground resistance can be reduced by the use of buried earth radials. Unless these are extensive, they are nowhere near as effective as a counterpoise. If we consider the antenna top load as one plate of a capacitor and the ground as another, by using a counterpoise we replace the ground plate with a copper wire.

The counterpoise can be a large web of wire insulated from the ground, but a simple "T" wire directly beneath the top load will produce considerable improvement. If the counterpoise is connected direct to the ground the antenna current will probably drop, indicating a loss rather than an improvement. The counterpoise must be tuned (Figs. 12a and 12b).

A counterpoise can be tuned by a variable inductance or variometer in series with the counterpoise and ground and in this mode it will be parasitic. The loading coils for the aerial and counterpoise must be adjusted alternately to obtain maximum aerial current. When correctly adjusted, the earth current should be small and the aerial current and counterpoise current similar. In practice an ammeter in the ground and counterpoise are unnecessary. Some other methods of tuning are shown in Figs. 12c and 12d which, when tuned correctly, should give zero ground current. These circuits are more difficult to tune than the parasitic counterpoise.

## REFERENCES

- Radio Engineers' Handbook, Terman, p. 772.
- Radiotron Designers' Handbook (fourth edition), Respective component of impedance, p. 903.

## Correspondence

Any opinion expressed under this heading is the individual opinion of the writer and does not necessarily coincide with that of the Publishers.

## MUNICH OLYMPIC DIPLOMA (M.O.D.)

Editor "A.R." Dear Sir,

I have been asked by Heiner DJ4KU and Maxie DJ4YL Balingen, of Munich, West Germany, to pass on information about a certificate called the Munich Olympic Diploma (M.O.D.). The rules for which are as follows:

"All contacts with stations in Munich from January 1, 1970, 0000 GMT to 2400 GMT the day of the official closing of the Olympic Games 1972 will count for this award. Munich stations are the members of the DOKs C00, C11, C13, C15, C16, C30. Contacts with Munich Amateurs count:

	DL/DJ/DK	Europe	DX
for phone	2 pts.	4 pts.	8 pts.
cw/rty	4 pts.	8 pts.	13 pts.

"Class I, 250 points; Class II, 300 points; Class III, 100 points.

"Mode: cw/phone/mixed. Bands: 160, 80, 40, 20, 15, 10, single band or mixed. The same station may be worked once per band any year. Fees: U.S. \$1.00 or 10 IRC. Send a list of the QSO details certified by two licensed Amateurs to: E. Misero, DJ8ZU, 8 München 13, Kreisinsstr. 6."

If DX operators who are interested in working for this award pass details of their call signs and anticipated operating times, days or dates and bands to me I will pass it on to my contact in Munich.

Incidentally, DJ4KU is blind, and as a consequence obtains a great deal of fun from Amateur Radio.

—S. T. Clark, VK3AHC.

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ETD 1170

Amateur Radio, June, 1971

## A SOLID STATE F.M. TRANSCEIVER—SOME AFTER-THOUGHTS

By G. L. C. JENKINS,<sup>†</sup> VK3ZBJ, and H. L. HEPBURN,<sup>‡</sup> VK3AFQ

Since the publication of an f.m. receiver design in the March 1971 issue of "A.R." and that for a companion transmitter in the April 1971 issue, some developments have taken place which may be of interest to readers.

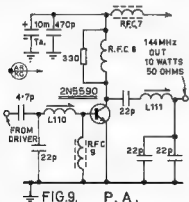
## ALTERNATIVE POWER TRANSISTORS

The transmitter design specified the use of a Motorola 2N5589 in the driver section and a Motorola 2N5590 in the p.a.

Varian P/L. of 679 Springvale Road, North Springvale, Vic., 3171 (and 3 Oxley Street, Crows Nest, N.S.W., 2065) suggested that their range of C.T.C. power devices made by the Elmac division of Varian in the U.S.A. might operate well in the circuit. Varian kindly provided a set of devices for trial.

A C.T.C. B3/12 was used in the driver section instead of a 2N5589 and gave somewhat better results. No changes were necessary either to board layout or component values. Used as an output stage on its own, the B3/12 gave well over 2 watts of output power for 70 mW. of drive. It would appear that the B3/12 can be used in the circuit as a direct replacement.

A C.T.C. B12/12 was used in place of the 2N5590 in the p.a. proper, but some component values needed changing. These changes are detailed below. After component optimisation, 15 watts of output were obtained from a 13.5 volt supply rail with 2 watts of drive—a considerable improvement over the 2N5590. At 15 watts out the total current drawn by exciter, driver and p.a. was 2.0 amps.



- FIG. 9. P. A.

Referring to Fig. 9, the following component changes are necessary to use the C.T.C. B12/12 in place of the 2N5590.—

- The series input capacitor is increased from 4.7 pF. to 6.8 pF.
- The 22 pF. capacitor between the input end of L110 and earth is reduced to 10 pF.

- (c) L110 is increased from 1½ turns to 2½ turns.
- (d) RFC8 is changed to 6 turns of No. 20 tinned copper wire, ½" i.d. and ¾" long.
- (e) L111 is changed to 3½ turns.
- (f) The 330 ohm load resistor across RFC8 is not needed.
- (g) The total fixed output capacitance of 44 pF. (2-22 pF. capacitors) to 36 pF. (2-18 pF. capacitors).

The only physical difference between the devices is that the Motorola transistors have a 3/8" diameter case while the C.T.C. transistors have a 5/16" diameter case. Connections are the same.

As a further experiment a C.T.C. B25/12 was driven by the complete transmitter and gave 30 watts of output at 146 MHz. The layout was the same as the existing p.a. but component values were different.

### CRYSTAL SPECIFICATIONS

Both transmitter and receiver use crystals in the series mode. With the transmitter especially, it should be noted that the trimming capacitor (and the variations in capacity brought about by the modulating process) are effectively in series with the crystal. When ordering transmitting crystals therefore, the supplier should be advised that they are for use in a series resonant circuit and that they should be calibrated with 25 pF. IN SERIES with the crystal and NOT (as is more normal) in parallel with the crystal.

### INCREASING EXCITER D.C. EFFICIENCY

As presented, the current drain of the exciter centres around 70 mA. with perhaps  $\pm 10$  mA. variation, depending on the spread of characteristics of the devices used.

This d.c. drain can be reduced to a mean value of 45 mA. for a constant r.f. output by some very minor modifications.

Firstly, the oscillator is removed from zener control and given the benefit of full supply voltage. Zener control is retained on the whole modulator section. The effect of this change is to increase the drive from the crystal oscillator. In turn, this increased drive causes the first two MPF121 doublers to saturate and "flat top".

Accordingly, the 47 ohm resistors in the sources of the MPF121 doublers need to be raised to around 330 ohms to bias back the MPF121s into an unsaturated condition. The exact value of source resistors for any individual case must be found by experiment. The simplest indication of arrival at the correct value is when the tuned cir-

cuits associated with each device tune sharply, there is a reduction in total current drain, and the output power remains constant. However the centre value of 330 ohms in each source suggested above will achieve a significant decrease in d.c. power requirements even if the maximum decrease is not achieved.

So far as the transmitter circuit board is concerned physical changes necessary are:—

- (a) Cut the h.t. line between the crystal oscillator and audio sections and bridge the cut with a 1.0K resistor.
- (b) Remove the original 330 ohm zener dropping resistor and replace with an RFC made by threading a single wire through a Neosid F29 slug.
- (c) Transfer the zener diode to a position alongside the 22K modulator trimpot.

## TRIMPOTS

The 1.5K and 22K trimpots used are the P.M.D. type made by Plessey/Ducon. They are obtainable from Radio Parts in Melbourne.

The mounting method favoured is to put three circuit board pins in the p.c.b. where the presence of the trimpot is required. The "legs" of the trimpot are bent back at an angle of about 45° and then soldered to the three pins in the board. The legs are bent in such a direction that the adjusting screw of the trimpot will face upward when the trimpot is mounted on the circuit board pins.

### TRANSMITTER BASE CHOKES

The "lossy" ferrite rod specified for the base chokes of the driver and p.a. are made by modifying 2½ turn RFCs marketed by the Philips organisation and having the type number 43/2020/38700. As supplied, these chokes consist of 2½ turns of thin tinned copper wire wound through holes in a cylindrical bit of ferrite. The choke is modified so that it consists of two single strands of wire, one strand of wire through each of two holes.

Additional holes are drilled in the printed circuit board about 1/8" away from the choke mounting holes already indicated on the p.c.b. The (four) wire ends of the modified chokes are threaded through the p.c.b., the choke body held hard on the board, and the wires pulled tight before soldering into place.

### CIRCUIT BOARD PREPARATION

Several instances have come to the notice of the authors where the printed circuit board, after drilling, has not been cleaned and protected against

(Continued on Page 12)

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# THE CLASS C RADIO FREQUENCY AMPLIFIER

LECTURE No. 13

C. A. CULLINAN,\* VK3AXU

The class C amplifier is used extensively in radio transmission and a good knowledge of its operation is essential.

By definition this is an amplifier in which the grid bias is appreciably greater than the cut-off value so that the valve plate current is zero when no alternating grid voltage is applied, therefore the plate current in a specific valve flows for appreciably less than one half of each cycle when an alternating grid voltage is applied.

The characteristics of a class C amplifier are high plate circuit efficiency and high power output.

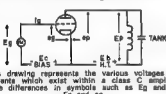
Because the plate current flows only over a portion of each cycle of the exciting grid voltage, the plate current takes the form of pulses and as described in Lecture 10 on Harmonics, the plate output contains considerable distortion.

Class C amplifiers are not used for audio frequency amplification, but when used as radio frequency amplifiers the plate current pulses are converted into sine waves in the amplifier's output circuit if it is properly designed. This action is known as the "fly wheel" effect.

In the discussion which follows, it is assumed that the grid and plate circuits of a class C r.f. amplifier are in resonance and are proportioned so that the radio frequency output of the amplifier will have minimum harmonics.

Also it is assumed that the amplifier has been neutralised if necessary, so that it is stable in operation.

Fig. 1 shows both the various voltage and current relationships which exist within the class C amplifier.



This drawing represents the various voltages and currents which exist within a class C amplifier. Note differences in symbols such as  $E_g$  and  $e_p$ ,  $E_p$  and  $e_p$ .

The following nomenclature is used:

$E_b$ —d.c. plate voltage.

$E_c$ —grid bias voltage.

$E_g$ —input grid wave (exciting grid voltage).

$I_g$ —peak r.f. grid current.

$E_p$ —voltage across output load circuit (tank circuit).

$I_b$ —d.c. plate current.

$I_p$ —peak r.f. plate current.

$e_p$ —output voltage, plate to cathode.

$e_p$  min.—minimum plate voltage ( $E_b - E_p$ ).

$e_g$  max.—maximum positive grid voltage ( $E_g - E_c$ ).

$e$ —plate operating angle.

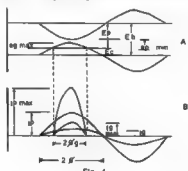
$\alpha$ —grid operating angle.

● Continuing the series of lectures by C. A. Cullinan, VK3AXU, at Broadcast Station 3CS for students studying for a P.M.G. Radio Operator's Certificate.

## IMAGES

In Fig. 1A  $E_g$  is the input voltage, assumed for purposes of simplicity to be a sine wave. This sine wave is impressed on the grid of the valve (between grid and cathode) along with the negative d.c. bias,  $E_c$ . This bias will be at least twice the value required for d.c. plate current cut-off. This bias may be obtained from a battery or other constant voltage source, from a grid leak, by the use of a resistor in the cathode of the class C amplifier valve or a combination of these methods.

In a communications continuous wave transmitter it is common to use a constant bias source and to key the transmitter in an earlier stage, thus the class C amplifier valve plate current will be cut-off during key-up conditions of signalling.



In A is shown a graphical representation of the voltages which exist within a class C amplifier. Note that the r.f. plate voltage  $E_p$  is 180 degrees out of phase with the grid exciting voltage  $E_g$ . In B is shown the relative amplitudes and angles of the flow of currents within a class C amplifier. Particular attention should be made of the plate current pulse which is converted into a sine wave in the "tank" circuit as described in the text.

Theoretically the correct class C bias should be sufficient to reduce the plate current to zero when no excitation is provided at the grid.

Sometimes the keying will be used to add extra bias, beyond the value of the positive grid voltage so that the plate current is reduced to zero. This is known as blocked grid keying. It is frequently used if the oscillator is on the same frequency and may not remain stable in frequency if keyed, i.e. grid excitation is present at all times.

Some types of variable frequency oscillators are very stable and grid-blocked keying of the oscillator may be used. Usually grid blocking voltage is applied to the oscillator and the class

C amplifier in such a way that the oscillator starts a fraction of a second ahead of the class C amplifier and stops just after the amplifier ceases to conduct. This sequence keying is done to prevent the transmission of "chirps" due to minute changes in frequency as the oscillator stops and starts.

When the class C amplifier is used in the plate modulated service for telephony it is usual to employ grid-leak bias, with a small amount of cathode bias as well.

Continuing with Fig. 1A, the a.c. voltage on the plate ( $E_p$ ) is superimposed on the d.c. plate voltage ( $E_b$ ). This is 180° out of phase with the grid voltage ( $E_g$ ).

Grid current flows in the grid circuit as soon as the positive portion of the exciting grid voltage equals the grid bias and plate current then starts to flow.

As the positive portion of the exciting grid voltage continues to rise, so does the plate current until the maximum exciting voltage is reached.

Then this voltage starts to fall and the plate current does likewise to the point where it becomes zero again as the positive exciting voltage reaches the same value as the negative grid bias.

During the rest of the exciting voltage cycle and the beginning of the next, no plate current will flow.

Thus for a sine wave input to the grid the signal in the plate circuit will be in the form of pulses.

This is shown in Fig. 1B which illustrates the relative magnitudes and angles of currents flowing in the circuit. This figure should be studied carefully.

As mentioned earlier, the pulses in the plate circuit will produce a considerable number of harmonics.

To convert these pulses to sine waves the output or "tank" circuit of the amplifier must have a large circulating current (r.f.) and to obtain this it is necessary to have a tank circuit with the proper Q or ratio of k.v.a. to k.w. that is the ratio of volt-amperes in the tank circuit to the d.c. plate power input.

For good harmonic reduction this ratio should be at least 12, although some designers might aim for ratios between 15 and 25.

## "FLYWHEEL" ACTION

The "flywheel" action of the tank circuit may be explained as follows:

For ease in understanding this, assume that the output "tank" circuit is in the form of a simple parallel tuned circuit.

When the a.c. exciting grid voltage ( $E_g$ ) goes positive, plate current ( $I_p$ ) flows in the "tank" circuit, being superimposed on the d.c. plate current, if the d.c. is fed through the inductance of the "tank".

The a.c. plate current ( $I_p$ ) flowing in the "tank" circuit produces an r.f. voltage across it, which charges the "tank" condenser, because in our dis-

\* 5 Adrian Street, Colac, Vic., 3250.

cussion we are dealing with radio frequencies, not audio frequencies.

Remember, too, from elementary theory that when current flows in a circuit it will produce a voltage across that circuit.

At the moment that the exciting a.c. voltage (Eg) starts to go negative, the condenser of the "tank" circuit starts to discharge towards the plate or anode end of the "tank" circuit to charge the other side of the "tank" condenser through the "tank" inductance.

When the exciting a.c. voltage (Eg) is negative no a.c. plate current (Ip) flows because the valve is cut off, but the "tank" condenser continues to discharge in the opposite direction through the "tank" inductance to charge the other side of the "tank" condenser.

This completes one cycle of the r.f. output and explains how an r.f. pulse in the anode circuit becomes a sine wave in the "tank" circuit.

This explains why it is possible to use a single valve or parallel valves as an r.f. amplifier in either class C or class B and obtain a sine wave output.

This cannot be done with audio frequencies.

Fig. 2 shows the wave forms of the voltages and currents in a class C amplifier, both unmodulated and modulated. These have been drawn to approximate the conditions which exist in the class C output stage of a 2 kw. broadcast transmitter, but are typical of all class C amplifiers.

## RATINGS OF VALVE

In working with class C amplifiers it is desirable to operate within the conditions set down by the valve manufacturer. Any attempt to exceed the published ratings will usually result in short valve life.

Usually two sets of ratings are published—the first known as C.C.S. means

Continuous Commercial Service and is the data used for the design of transmitters which operate more or less continuously. I.C.A.S. is the term used for the second set of ratings and means Intermittent Commercial and Amateur Service. These ratings have been devised on the basis that in I.C.A.S. the users will take a long period of time to obtain the same use or life from a valve that is obtained by a user under the C.C.S. rating and this is the reason that the I.C.A.S. ratings are higher than for C.C.S.

To illustrate this, here is some data taken from an R.C.A. valve data sheet for valve type 833A:—

**Service:** R.f. power amplifier or oscillator, for class C telephony or class C f.m. telephony. Forced air cooling.

Typical Operation:	C.C.S.	I.C.A.S.
D.c. plate voltage	4,000	4,000 V.
D.c. grid voltage	-200	-255 V.
Peak r.f. grid current	375	415 V.
D.c. plate current	450	500 mA.
Power output	(approx.)	1,440 1,800 W.

If a class C r.f. amplifier is to be modulated then it is necessary to reduce the ratings from those shown above to prevent damage to the valve.

**Service:** As a plate modulated r.f. amplifier for class C telephony, the data becomes (forced air cooling):

Typical Operation:	C.C.S.	I.C.A.S.
D.c. plate voltage	3,000	4,000 V.
D.c. grid voltage	-900	-325 V.
D.c. plate current	415	450 mA.
Power output	(approx.)	1,000 1,500 W.

The ratings for natural air cooling are considerably reduced from those for forced air cooling.

The above data shows that for C.C.S. class C plate modulated telephony the d.c. plate voltage has been reduced from

4,000 volts to 3,000 volts and the approximate power output drops from 1,500 watts to 1,000 watts. Also note that for frequency modulation the C.C.S. power output is approx 1,440 watts. This is because for f.m. the carrier power remains constant whereas for a.m. it varies with modulation as explained previously.

Here at 3CS we operate our class C modulated amplifier with four 833A valves in parallel, under C.C.S. ratings.

Examination of the valve life cards, recorded over 15 years, shows that the average life of an 833A valve is 10,000 hours. This includes failures from all causes. The manufacturers guaranteed valve life is 1,500 hours.

In many cases the valves are withdrawn between 10,000 and 12,000 hours use because the harmonic distortion at 3 KHz. to 5 KHz. increases to the allowable limits or because emission of the cathode falls off so that full modulation is not possible on positive peaks (lack of positive peak emission), resulting in asymmetrical modulation.

This falling off of positive peak emission is detected with an amplitude modulation meter and a low distortion audio frequency oscillator, usually long before the modulated amplifier plate current meter shows a reduction of plate current brought about by severe loss of emission.

## W.I.A. D.X.C.C.

Listed below are the highest twelve members in each section. Position in the list is determined by the first number shown. The first number represents the participant's total countries less any credits given to a district committee. The second number shown represents the total D.X.C.C. credits given, including deleted countries. Where totals are the same, listings will be alphabetical by call sign.

Credits for new members and those whose totals have been amended are also shown.

PHONE			
VK5M9	318/343	VK4FJ	287/307
VK8RU	317/343	VK4TY	284/288
VK3AO	311/338	VK3APK	281/287
VK6MK	304/334	VK2AAK	274/279
VK4KS	302/317	VK3TL	271/277
VK5AB	297/314	VK4UC	270/270

Cert. No.	Call	Total
117	VK3KM	203/301
118	VK3APU	114/114

Amendments:			
VK3ZE	288/371	VK3AMK	230/230
VK4PX	250/280	VK4XJ	189/183

C.W.			
VK3QL	303/330	VK3NC	274/300
VK3AHQ	301/315	VK3XB	270/287
VK4PJ	280/315	VK3ARK	270/279
VK3AGH	282/285	VK3RU	268/269
VK3YL	281/288	VK4TY	255/272
VK3APK	250/288	VK3TL	255/280

Cert. No.	Call	Total
86	VK4KX	178/178

Amendments:			
VK4UC	176/177	VK4XJ	139/145

OPEN			
VK6RU	318/343	VK4KS	303/322
VK3AGH	314/334	VK3EO	302/325
VK3VN	311/323	VK3ARX	296/308
VK3SD	305/321	VK3APK	286/309
VK4TY	306/321	VK4EJ	256/323
VK6MK	304/324	VK3SG	294/300

New Member:		
Cert. No.	Call	Total
131	VK3APU	118/118

118	VK3APU	118, 119	
Amendments:			
VK4UC	293/294	VK4XJ	194/201
VK4PX	270/273	VK3AMK	122/125

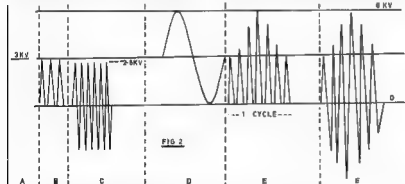


Fig. 2—Wave forms existing in a class C amplifier in a typical transmitter

A.—D.c. plate voltage, unmodulated, 3 KV.

B.—R.f. current pulses in the plate circuit, unmodulated (peak 10 amp.).

C.—R.f. voltage across the "tank" circuit. The current pulses shown in B have been converted into sine waves in the "tank" circuit because of the "flywheel" action of the "tank", as explained in the text. This drawing is of the voltage that has been produced across the "tank" circuit. By calculation it is 2.5 KV for this particular transmitter.

D.—Modulated plate voltage. This comprises the audio frequency modulating voltage superimposed on the d.c. plate voltage. That is above the 3 KV axis, B plus a.c. modulation voltage, so that peak positive voltage rises to 5 KV. Below the 3 KV. axis, B minus a.c. modulation voltage, so that peak negative voltage drops to zero.

E.—R.f. current pulses in the plate circuit during modulation. The peak positive pulse rises to 2 amps and on the negative half of the modulating wave the current drops to zero.

F.—The modulated voltage produced across the "tank" circuit because of the "flywheel" action because of the small size of the drawings it is not possible to show the r.f. current pulses and resultant sine wave voltages as sine waves, this being the reason that they are drawn in the manner shown.



## F.M. TRANSCEIVER

(Continued from Page 2)

oxidation. The effect of these omissions has been to lead to suspect soldered joints and the near impossibility at any later stage to change components, or in any way carry out modifications or repair work.

It is strongly urged therefore that any printed circuit board be cleaned and protected before any soldering work is carried out. This comment does not, of course, apply to boards which have been solder rolled during manufacture.

The simplest way to clean copper circuits boards after drilling is to polish with fine steel wool such as "Jex". Immediately after polishing the clean copper should be given a light coating of clear lacquer. The one recommended is the "metal finish clear" "Spray Pak" put out by Balm Paints under the "Dulux" trade mark.

It is quick drying and (provided a heavy application has not been given) the thin film of lacquer can be soldered through with impunity. Boards treated in this way by the writers are still clean and unoxidised after two years' service and still accept solder as well as the original clean copper.

### TUNING UP THE EXCITER

As an alternative to the procedure set out in the April 1971 "A.R." for tuning up the oscillator and doubler stages of the exciter, the following simplified procedure is offered.

It is based on the fact that as the crystal comes into oscillation drive will be applied to the first MPF121 doubler, causing its operating current to rise. As the first doubler starts to put drive into the second doubler, it, in turn, will draw more current. In both doublers there is a by-passed source resistor, the voltage drop across which will rise as drive increases.

Thus the alternative tuning procedure consists simply of putting a high resistance voltmeter or v.t.v.m. on, say, the 5-volt range, across the source resistor of the first MPF121 and adjusting the slugs of L101 and L102 for maximum voltage indication.

The process is repeated with the voltmeter across the source resistor of the second MPF121 doubler, this time adjusting the slugs of L103 and L104 for maximum indication.

It is still necessary to use some form of power meter or r.f. indicator to tune up the MPF121 amplifier.

### SIGNAL SOURCE FOR RECEIVER LINE UP

The performance of the receiver is such that to obtain best results the signal level used for final lining up must be very low. Large signals (i.e. 2-3 microvolts or more) cannot successfully be used for final lining up since they cause the whole receiver to saturate.

In the absence of a signal generator with an accurate low level attenuator capable of going down to 0.2/0.3 microvolts, then the simple signal source described by Ron Higginbotham, VK-

3RN in the December 1970 issue of "A.R." is recommended. Several people in the Melbourne area have made up this device using transmit crystals from existing carbonphones to provide the correct frequency.

If the coupling capacitor between the "High" and "Low" outputs is removed the amount of signal available from the "Low" output terminal appears to be suitable for final lining up of the receiver described.

### NEW CALLING, EMERGENCY or SKED-MAKING FREQUENCY 7050 KHz.

Whenever you are in the shack and not operating, keep the receiver running on 7050 KHz.

### NEW PROVISIONAL UNSPOT NUMBERS

FEBRUARY 1971

Dependent on observations at Zurich Observatory and its stations in Locarno and Arosa.

Day	R	Day	R
1	— 77	15	— 66
2	— 76	16	— 66
3	— 68	17	— 62
4	— 80	18	— 63
5	— 63	19	— 87
6	— 78	20	— 91
7	— 70	21	— 91
8	— 80	22	— 100
9	— 37	23	— 87
10	— 37	24	— 96
11	— 66	25	— 99
12	— 66	26	— 69
13	— 63	27	— 66
14	— 60	28	— 71

Mean equals 71.5  
Amended Smoothed Mean for July 1970: 105.3

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# AUSTRALIAN 2 METRE F.M. REPEATER DIRECTORY

# NEW CALL SIGNS

JANUARY 1971

The Australian development of f.m. repeaters has been along the agreed two-channel principle on Channel 1 (148.1 in and 145.5 out) and Channel 4 (148.4 in and 145.9 out). The simplex operation is Central Channel B (146.0), Channel A (145.854) and Channel C (146.148). The system is based upon a 60 KHz. channel spacing with  $\pm 15$  KHz. deviation.

## OPERATIONAL REPEATERS

### New South Wales:

**Sydney**—Channel 4, VK2BWI/R1, at Dural. Tx STC base, 40 watts to ground plane at 57 feet. Rx AWA MR20B, ground plane at 57 feet. Separation 250 feet. Coverage approx. 60 miles.

**Central West (Orange)**—Channel 1, VK2AOA/R1, at Mt. Canobolas. Note: Output is currently on 145.854 but this will be changed to 145.6 later this year. Tx AWA base 50 watts to ground plane. Rx AWA, ground plane, both 20 feet high. 400 yards separation. Coverage 100 miles.

### Victoria

**Melbourne**—Channel 1, VK3WI/R1, at Carlton. Tx STC 128 base, 50 watts output. Rx is solid state STC 131 with equipment to prevent Tx lock-up in event of Tx failure. Both antennas are 45° ground planes, 250 feet high with a separation of 600 feet. Coverage approx. 25 m.

**Geelong**—Channel 4, VK3BGL/R2 located at Gnarwarre. Solid state home-brew equipment. Power output 25 watts. Tx antenna is a folded dipole (temporary) 50 feet up, and receiving is four stacked dipoles 100 feet high. Coverage approx. 60 m.

**Gippsland**—Channel 4, VK3V1/R3, temporary location at Mt. Bess (near Moe), future permanent location at Mt. Tassie. Solid state I.G.L. equipment, power output 4 to 6 watts. Both antennas are half wave dipoles, receiving 50 feet high, transmitting 35 feet high.

### Queensland

**Gold Coast**—Channel 1, VK4EI/R3, at Mt. Tamborine. Solid state rx, tx home-brew, 25 watts. Antenna 5 x half wave collinear at 40 feet for tx and rx, 250 yards separation. Coverage 50 miles.

### South Australia

**Adelaide**—Channel 4, VK5WI/R1, at Craferia. Tx TCA 1680 solid state 15 watts, rx TCA 1675/777 solid state. Antennas ground plane with small vertical separation. Coverage appears good.

## REPEATER APPLICATIONS PENDING

VK2—Newcastle, Mt. Sugarloaf, Ch. 4.  
VK6—South Eastern (Albany), Mt. Barker, Ch. 4.

VK7—Northern Tas., Mt. Barrow, Ch. 4.  
Hobart, Mt. Wellington, Ch. 1 or Ch. 3.

## PLANNING STAGES

- VK2—Central Coast, Gosford, Ch. 1.  
South Coast, Wollongong, Ch. 1.  
Murrumbidgee, Wagga, Ch. 1.  
Murray, Albury, Ch. 4.
- VK3—North West, Mildura, Ch. 4.  
Central—Bendigo, Ch. 4.
- VK4—Brisbane, Mt. Cootha, Ch. 4.
- VK6—Perth, Tuart Hill, Ch. 4.

## CHANNEL ALLOCATIONS FOR POSSIBLE FUTURE DEVELOPMENT

- VK1—Canberra, Ch. 4.
- VK2—North West, Mt. Kaputar/Narrabri, Ch. 1.  
Far West, Cobar, Ch. 1.  
Warrumbungle, Coonabarabran, Ch. 4.  
Riverina, Griffith, Ch. 4.  
Snowy Mts., Far South Coast, Ch. 1 or 4.  
Mid North Coast, Port Macquarie, Ch. 1.  
Far North Coast, Grafton, Ch. 4.
- VK3—Western, Hamilton/Horsham, Ch. 1.  
Northern—Shepparton/Wangaratta, Ch. 1.
- VK4—No details known, Ch. 1.
- VK5—No further plans at the moment.
- VK6—At this stage all possible sites will use Ch. 4, e.g. Narrogin/Wagin; Bunbury/Busselton.

VK7—North West, Burnie/Devonport, same channel as finally used by Hobart.

## PROJECT AUSTRALIA EXPERIMENTAL REPEATERS

The Australia experimental systems which have the blessing of the P.M.G. Department are designed as a service to enable Amateurs to adjust their equipment in preparation for AOE. It is emphasised that this is not part of the overall repeater plan.

It is possible that similar equipment will be constructed and forwarded to Divisions for use by Amateurs in other States.

One experimental repeater is located at Mt. Dandenong (Vic.). The input frequency is 145.76 MHz. and the output frequency is 432.3 MHz. I.G.L. equipment is used. The transmitter output power is 10 watts. Both antennas are quarter wave dipoles about 20 feet high with vertical polarisation in, and, temporarily, vertical polarisation out (this may be horizontal by the time this goes to press).

The other experimental repeater (also I.G.L. equipment) is located at Mt. Bess (near Moe, Vic.). The input frequency is 147.76 MHz. and the output frequency is 432.2 MHz. The transmitter output power is 4 to 6 watts. Both antennas are about 15 feet high. The receiver uses a 5/8 co-ax. dipole (vertical polarisation), and the transmitter a 42 element collinear (horizontal polarisation).

- VK3ZJY—J. C. Foster, 28 Avenue Rd., Moanman, 2088.
- VK3ZUD—J. O. King, 18 Darnley St., East Gordon, 2075.
- VK3ZUR—N. Flores, 6 Pamela Pde, Emu Plains, 2700.
- VK3ZUW—P. C. Wals, 46 Arthur St., Randwick, 2031.
- VK3ZUH—J. E. Luksey, 1 Blenheim Pl., Glenfield, 2107.
- VK3ZUR—R. Eccleston, 3 Valerie St., Mt. Pritchard, 2170.
- VK3ZUR—R. Carr, 275 Main Rd., Toulkley, 2282.
- VK3ZUR—D. J. Turner, 58 Amor St., Hornsby, 2077.
- VK3ZUR—R. G. Swadling, 3 Grafton St., Lawrence, 2460.
- VK3ZUR—G. K. Wilson, 60 River St., Kempsey, 2440.
- VK3ZUR—E. S. Turner, 25 Amor St., Hornsby, 2440.
- VK3ZUR—E. M. van de Weyer, 101 Francis St., Bondi, 2028.
- VK3ZUR—W. E. C. Bennett, 5 Hurn St., New Lambton, 2305.
- VK3ZUR—O. W. Guy, 34 Peter St., Box Hill North, 3185.
- VK3ZUR—E. Russell, 104 Kangaroo Rd., Oakleigh, 3186.
- VK3ZUR—P. E. Lamb, 28 Panoramic Gr., Glenview, 3100.
- VK3ZUR—P. M. Wrobel, 36 Elton St., Glenroy, 3104.
- VK3ZUR—S. G. Bushell, 35 Church St., Bayswater, 3105.
- VK3ZUR—C. Buckley, 1/5 Carmichael St., West Footscray, 3012.
- VK3ZUR—J. W. Tomlinson, 66 Doncaster Rd., North Balwyn, 3104.
- VK3ZUR—L. James, 50 Combermere St., Essendon, 3040.
- VK3ZUR—R. C. Coast Radio Club, P.O. Box 248, Southport, 4215.
- VK3ZUR—F. J. Miller, 23 Gladstone St., Coorparoo, 4150.
- VK3ZUR—D. G. Hopkins, 11 Stephen St., Morningside, 4170.
- VK3ZUR—D. McWilliam, 3 Rosemary Ave., Mt. Ida, 4055.
- VK3ZUR—G. E. Millward, 4 Mourilyan Rd., Mourilyan, 4895.
- VK3ZUR—J. W. Hennessy, 233 Chapel Hill Rd., Kenmore, 4099.
- VK3ZUR—A. F. Harley, 23 Princess St., Croydon, 3130.
- VK3ZUR—M. Morris, Flat 30, Harcourt Ave., Modbury, 5062.
- VK3ZUR—W.A.L.A. S.A. Division Inc., Station: Hillcrest, 5115, Craferia, 5115. Postal: G.P.O. Box 1894K, Adelaide, 5001.
- VK3ZUR—W. D. Moulton, 18 Stanley St., Plympton, 5097.
- VK3ZUR—J. C. Merry, 34 Davidson Rd., Elizabethville, 5113.
- VK3ZUR—B. D. Norman, Station: Yahi, via Mt. Gambier, 5200. Postal: P.O. Box 171, Mt. Gambier, 5260.
- VK3ZUR—R. W. Walker, 5/378 Scarborough Beach Rd., Scarborough, 5113.
- VK3ZUR—E. S. Harrison, Flat 7, Mitchell Court, 15-17 Mary St., Highgate, 5100.
- VK3ZUR—N. Stephen, 19 Lalle St., Cannington, 6187.
- VK3ZUR—D. W. Bridge, 100 Hlg. Sq., Vincent St., Leederville, 6007.
- VK3ZUR—P. Canavan, 55 Grand Promenade, Baywater, 6001.
- VK3ZUR—M. W. Dunning, 46 Holmesdale Rd., 6001.
- VK3ZUR—J. W. Wade, Station: O.T.C. (A), Carnarvon; Postal: P.O. Box 56, Carnarvon, 6701.
- VK3ZUR—G. M. Ranft, 10 Lansdowne Cres., West Hobart, 7000.
- VK3ZUR—L. Hester, 34 Stanley Cr., Alice Springs, 9700.
- VK3ZUR—R. H. Whellum, Explained Hostel, Explained, Darwin, 2792.

## CANCELLATIONS

- VK1JR—J. R. Watson. Not renewed.
- VK1ZAB—G. W. Fletcher. Not renewed.
- VK1ZED—E. J. Barnes. Not renewed.
- VK2AF—P. E. Staley. Not renewed.
- VK2AP—M. Burton. Not renewed.
- VK2BP—S. R. Pedemont. Deceased.
- VK2ZL—L. S. McKeechie. Not renewed.
- VK2ZUR—G. A. Fuchet. Not renewed.
- VK2ZUR—A. R. Marjoram. Not renewed.
- VK2ZUR—Sydney Teachers' College Radio Club, 2001.
- VK3QZ—J. G. Colley. Not renewed.
- VK3ZV—J. F. Howarth. Deceased.
- VK3ZUR—M. Weeks. Not renewed.
- VK3ZUR—K. O. Phillips. Not renewed.
- VK3ZUR—W. D. Mather. Transferred to Qld. (Continued on Page 37)

# VK-ZL-OCEANIA DX CONTEST, 1970 RESULTS

## AUSTRALIA

### Phone Section

Call Sign	80	40	20	15	10	Total
AK1GID	—	475	1180	8175	6435	24345
AK1JBC	480	110	5665	2670	1150	10630
AK1AOP	—	2315	1440	1383	3040	—
AK1KMK	423	8335	10390	7220	6040	26700
AK1APK	375	2985	10035	6273	5885	25555
AK1XCT	—	11745	4815	3885	30455	—
AK1WVC	—	8745	4555	3615	12415	—
AK1XRC	270	—	6545	—	—	6545
AK1AOU	—	2575	625	300	3730	—
AK1BAA	—	3700	—	—	3700	—
AK1BDN	—	3620	—	—	3620	—
AK1AMH	—	3015	330	570	3895	—
AK1BNC	565	2315	—	—	3290	—
AK1ABC	—	—	8770	3770	12540	—
AK1UJ	575	—	1490	—	4485	—
AK1KMK	—	11645	2675	3270	10790	—
AK1QV	445	—	3580	—	6405	10410
AK1ASU	—	8380	—	—	8380	—
AK1BKS	—	3035	—	4795	7830	—
AK1ASV	570	110	1630	3265	6210	11695
VK1BBA	—	5045	—	—	5045	—
AK1SM	—	—	5245	—	5245	—
AK1ABA	—	—	6155	—	6155	—
AK1ARV	—	3535	—	—	3535	—
VK1BCL	630	—	—	—	630	—
AK1ALT	—	7270	3185	6910	14465	—
AK1AFV	365	88	1678	8380	12570	—
AK1AVX	—	—	11615	11615	—	—
AK1BPF	—	—	10720	—	10720	—
VK1EJ	—	1285	—	—	1285	—
AK1WJ	210	—	1635	1880	3240	5765
AK1AL	188	—	3330	1745	628	5783
AK1XJ	—	—	3800	—	3800	—
VK1QJ	—	3875	—	—	3875	—
AK1UA	—	1190	1500	—	2690	—
AK1QA	—	800	158	—	958	—

AK1SWP	—	4105	5050	8375	14418	—
AK1SFO	480	495	8075	3735	5230	12108
AK1EZE	—	8650	—	—	8650	—
VK1BZX	—	1295	78	—	1373	—
AK1CT	185	5415	5545	6630	9040	24390
AK1BUB	330	315	4090	3945	5880	15818
AK1HDD	—	—	3290	3115	13625	13625
AK1LKL	—	3290	3115	6380	10005	—
AK1TKK	265	805	11340	6440	4375	23145
AK1TVJ	—	1800	—	—	1800	—
AK1AZ	—	10490	685	635	3310	—
AK1GZ	—	305	10405	9615	7685	25340
AK1UL	—	9415	515	765	3390	—
AK1XK	—	1600	1985	3685	7270	—
AK1KJ	—	8130	—	—	8130	—

### C.w. Section

Call Sign	80	40	20	15	10	Total
AK1APK	285	1815	9415	8290	3090	29945
AK1WV	—	1580	1810	2465	1590	7445
AK1GR	210	960	6355	1525	2535	13345
AK1VRN	835	1895	2540	3715	1040	10535
AK1BBA	—	—	4555	—	4555	—
AK1BBA	—	3035	545	—	3170	—
AK1BBA	—	2340	530	190	3480	—
AK1UJ	—	780	—	—	780	—
AK1ABC	—	620	—	—	620	—
AK1OP	—	1835	6110	4415	13680	—
AK1AXK	—	—	8245	—	8245	—
AK1APN	1160	1660	6485	—	10028	—
AK1XK	810	—	—	8805	9415	—
VK1MR	—	5550	—	—	5550	—
AK1MJ	—	—	4655	—	4655	—
AK1ARV	—	—	4195	—	4195	—
AK1ABA	—	—	3390	—	3390	—
AK1RJ	—	—	618	—	618	—

AK1VX	—	—	9615	—	9615	—
AK1UA	—	4175	2130	—	6305	—
VK1EJ	—	2320	—	—	2320	—
VK1XK	—	1260	2410	1160	388	2223
AK1XJ	—	—	4895	—	4895	—
AK1SFO	—	860	8235	3450	—	12545
AK1SFR	615	1790	7065	—	8940	—
AK1BPM	—	—	4805	1985	7790	—
AK1BS	100	—	545	610	385	1640

AK1EHD	—	1370	3415	10115	6405	26820
AK1EPL	—	110	110	3330	2585	3715
AK1TKK	—	1380	2030	8575	4875	28935
AK1EHA	—	—	1940	1590	3115	6975
AK1XGN	—	—	—	—	9950	9950
VK1XK	—	—	6320	3310	345	8975

## VK S.w.I. Section

Phone	C.w.	Total
P. Vernon, L2295	10330	4500
K. Neal, L2419	—	410
C. Ferguson	—	410
R. Tremayne, L3385	12285	8510
E. Treblehorn, L3945	—	4310
K. Cunningham, L4104	—	5370
P. Drew, L4021	—	8185
R. Mullon (VK7)	—	16330
R. Everett, L7043	—	10570

## NEW ZEALAND

### Phone Section

Call Sign	80	40	20	15	10	Total
ZM1AKZ	—	385	4170	8190	5150	17895
ZL1AGU	1350	1305	7835	2885	2330	13895
(includes 100 pts. on 180 max)	—	—	—	—	—	—
ZM1AIZ	580	785	3300	2855	3700	12130
ZM1AIV	580	—	2505	8715	—	11140
ZM1AAS	—	81	1030	—	1030	—
ZM1AVO	—	81	8425	—	8425	—
ZM1AMM	—	4270	1410	—	5680	—
ZM1ARO	—	1740	—	3650	5390	—
ZM1ACW	—	3870	—	—	3870	—
ZM1YB	—	—	1305	625	3130	—
ZM1AVV	—	9435	1290	—	10745	—
ZM1QK	—	6385	1215	—	7601	—
ZM1QK	—	4655	—	—	4655	—
ZM1BCK	—	6090	—	—	6090	—
ZM1AWH	1800	—	—	—	1800	—
ZM1OUB	—	7670	370	—	8040	—
ZM1QK	—	4655	—	—	4655	—
ZM1QZ	580	7975	6100	2300	17855	—
ZM1AOS	305	8780	5370	—	14555	—
ZL1AH	—	9435	—	—	9435	—
ZL1MY	625	3235	—	—	3860	—

### C.w. Section

Call Sign	80	40	20	15	10	Total
ZM1HV	100	320	5775	5815	2245	12355
ZM1AV	—	—	11285	—	11285	—
ZL1BV	—	1015	10715	—	10715	—
ZL1UQ	51	101	1345	3435	1690	3041
ZM1AIZ	51	1700	3700	3090	1705	10715
ZM1QK	—	—	2580	1865	3630	6075
ZM1AKM	275	—	5415	2040	—	6330
ZM1IL	—	—	6185	3610	8190	—
ZM1AIV	—	180	2035	675	1335	3945
ZM1BWN	—	—	1325	—	1325	—
ZM1ARV	—	—	1325	—	1325	—
ZM1BHQ	1090	—	7585	2710	12390	—
ZL1BSC	—	3085	2865	6145	10950	—
ZL1APZ	—	—	2865	6145	9010	—
ZM1QK	—	—	5235	3235	8470	—
ZM1AH	—	1495	1335	—	2830	—
ZM1AWH	—	—	8705	—	8705	—
ZM1QK	155	—	8725	—	8880	—
ZM1QK	—	—	8945	—	8945	—
ZM1AT	—	2665	4650	—	7315	—

## OVERSEAS

### Phone Section

Call Sign	80	40	20	15	10	Total
DJ1FH	4907	718M	—	—	702	5627
KH1OMP	36830	WCHW/KG8	—	—	680	37510
KH1GJ	31400	PK1AR	—	—	680	32080
KH1XK	15530	—	—	—	—	15530
CT1LN	—	321	—	—	—	321
DJ1FH	10815	718M	—	—	702	11527
DJ1LK	9054	ONM8G	—	—	3705	12759
DJ1AA	7120	OZTKB	—	—	743	7863
DJ1PC	5823	OZ1PO	—	—	5823	5823
DJ1UP	1581	P4001	—	—	1581	1581
DJ1AUF	1682	P4012C	—	—	234	1916
DJ1YF	134	PA1JML	—	—	78	212
E1AFK	128	PK1CCK	—	—	4384	4512
E1AKG	182	PK1CCK	—	—	2040	2222
E1ASB	188	SM1ANB	—	—	—	188
E1ACW	53	SM1YVB	—	—	1428	1481
E1RIM	1581	P4001	—	—	1581	1581
G1PHO	1680	SM1MC	—	—	828	2508
G1CN	1458	SM1BUB	—	—	—	1458
H1AKG	81	SM1OB	—	—	265	346
H1AMH	30	SM1ABL	—	—	328	358
H1BAA	3265	SM1VB	—	—	780	4045
H1BUD	1840	SP1ABE	—	—	1380	3220
IL1AA	1580	SP1CQM	—	—	1580	1580
IL1AT	1840	SP1RH	—	—	1840	1840
IL1AJ	965	SP1AGH	—	—	965	965
LA1OI	788	SP1RKH	—	—	788	788
LA1QK	1328	SP1BFL	—	—	1328	1328
LZ1KAA	34	SP1CTN	—	—	12	46
OR1RH	382	SP1EER	—	—	2	384
OR1YS	30	—	—	—	—	30

## Asia (excluding Japan)

KP1BQ	—	5480	OD1BA	—	34
KP1BQ	—	5480	ZC1MT	—	512

## Japan

JAB1DT	690	JAA1AA	3468
JAB1DX	443	JAA1TW	2185
JAB1AM	306	JAB1RB	1119
JAB1EZ	30	JAB1PD	1169
JAB1CA	9621	JAB1EJ	9621
JAB1VS	2815	JAB1ND	728
JAB1AT	2587	JAB1LU	445
JAB1UC	2587	JAB1LT	545
JAB1RU	1630	JAB1NO	10535
JAB1TR	1464	JAB1XW	5180
JAB1NF	1500	JAB1FM	3528
JAB1TR	84	JAB1EJ	2763
JAB1EJ	350	JAB1FE	1638
JAB1AS	430	JAB1VP	434
JAB1EJ	80	JAB1DZ	88
JAB1GZ	300	JAB1AD	2975
JAB1QU	147	JAB1QR	1180
JAB1EJ	350	JAB1DM	16000
JAB1RN	87	JAB1AD	1023
JAB1OY	12	JAB1EM	220
JAB1EJ	2018	JAB1EJ	2018
JAB1NF	5083	JAB1KD	1183
JAB1NF	1413	JAB1TA	1183
JAB1NF	508	JAB1KR	1183
JAB1NF	810	JAB1EJ	1285
JAB1NF	810	JAB1BA	8274
JAB1NF	284	JAB1EV	870
JAB1NF	188	JAB1TD	617
JAB1NF	188	JAB1EJ	1285
JAB1NF	88	JAB1YA	1728



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# AUSTRALIS BALLOON FLIGHTS—A PRELIMINARY REPORT

By RICHARD TONKIN\*

This article represents a preliminary report on the results of the recent flights of the Australis translator system on balloon packages. Because all of the tapes and other data from the flights has not yet been analysed, a complete list of the Amateurs who worked through the package, and further details on the results of the flights will be held over until the next issue of "A.R."

The main reasons for conducting the balloon flights with the Australis translator were to demonstrate its operation over relatively long distances and to experiment with antenna systems which could be used on any future flights. The translator used was a prototype of one of the four channels which, if all goes well, will fly on the A-O-B satellite next year. The translator was built by Les Jenkins, VK3ZBJ. Its input was 146.00 MHz. (Channel B, f.m.), with the output on 432.30 MHz. The power output was approximately 500 milliwatts. Prior to the balloon flights, the translator had been operated for several weeks on top of Mt. Dandenong, near Melbourne, and a considerable amount of interest was shown by Amateurs in this test.

Permission was obtained from the Department of Supply to fly the translator as a "piggyback" experiment on the March-April series of scientific research balloon flights from Mildura, about 350 miles north-west of Melbourne. The balloon series, called HIBAL, consisted, so far as the Australis translator package was concerned, of four flights, to 70,000 (70K), 90,000 (90K), 105,000 (105K) and 120,000 (120K) feet.

The balloons are several hundred feet high when launched and they gradually assume a spherical shape as they rise into the upper atmosphere. The payload, or gondola, consists of a tubular steel frame inside which the equipment is located. The gondola is about the size of a small car, and weighs an average of about 500 lbs.—so HIBAL is no mean balloon!

After launch from Mildura airport, the helium-filled balloon rises at a rate of about 1,000 feet per minute until it reaches its float altitude. The length of time that the balloon and its payload float depends on the type of experiment being flown, but two to three hours was the average float time for the four flights on which the Australis package was hitching a ride. At the end of the float period, a radio command transmitted to the gondola from the HIBAL control station at Mildura airport separates the balloon from the gondola. As the gondola drops into the denser layers of the atmosphere, a parachute opens and lowers the payload to the ground. A chase aircraft follows the gondola's descent and radios its landing position to HIBAL Land-Rovers which travel to the landing site and recover the payload.

George Long, VK3YDB, who prepared the translator for the flights, and I travelled to Mildura before the first flight to test the translator with the HIBAL packages, settle the final flight details with the HIBAL personnel and meet the Amateurs at Mildura who had previously offered their help with the flights. The Amateurs who assisted the flight at Mildura included Mike VK-3CCX, who was a real tower of strength and who, being a member of the HIBAL crew, was able to give invaluable technical assistance on the four flights; Noel VK3AGF, who did a fine job in communicating with the anxious project members in Melbourne; Graham VK-3YEJ, Joan VK3YEK and her OM, Ray VK3ZBN. Without the seemingly tireless help of these people, it would not have been possible to fly the Australis translator on the HIBAL flights.

The four flights were launched at about dawn on 23rd March (70K), 25th March (105K), 2nd April (90K) and 5th April (120K). All flights rose to their planned altitudes and the translator worked well on the four trips it took into the stratosphere. The same translator unit was used on each flight and it was recovered undamaged after each flight. Before the flights began, it had been calculated that the Mildura launch site and the planned float altitudes would allow Amateurs in Adelaide and Melbourne (and points in between) to maintain contact during the ascent and float phases of the flights. We were a little more optimistic about the 120K flight and we hoped, because of the greater altitude it would reach, that we may be able to get signals into it from further afield than Melbourne.

In the event, Adelaide-Melbourne (and vice versa) QSOs were achieved on all four flights. The copy varied from unreadable to numerous dBs over S9, depending on the power that the transmitting station was putting into the translator, how many people were trying to get into it at the same time, and the orientation of the antenna system on the gondola. The 2 metre receive aerial was a vertical ground plane and the 432 MHz. transmitting antenna was an omni-directional turnstile. For the 70K and 120K flights, the antenna system was mounted on the top of the HIBAL gondola and on the 105K and 90K flights it was located on the bottom of the gondola. These were the two most convenient positions to put the antennas, having regard to the need to keep the Australis aerials away from the HIBAL equipment and taking into account the shadowing effect which the gondola frame and the HIBAL experiments had on the Australis antenna radiation patterns.

The results from the four flights was very interesting and it appears, from initial data that have been looked at, as though the top-located antennas (70K and 120K flights) operated better than the bottom-mounted ones (105K

and 90K flights), at least so far as Melbourne Amateurs were concerned. It is possible that atmospheric temperature inversions played a part in some of the long signal fades which occurred during the flights. It is hoped that a more complete report on these aspects of the flights can be included in a later issue of "A.R."

The following is a preliminary list of Amateurs who worked through one or more of the translator flights. As mentioned above, this is not a complete list and represents only the call signs heard on some of the tapes of the flights. The complete list and more details of each flight will be in July "A.R."

VKs 5ZDR, 6NZ, 6QZ, 6ZK.

VKs 3ZCE, 3YFL, 3FW, 3YBO, 3ZBJ, 3YDB, 3AGF, 3YEJ, 3ASV, 3AKC.

VKs 1VP and 2ZHM.

There are probably at least another six VKs calls who worked through the translator and a couple of other VK3 ones as well. It would be a great help if the people who worked through it would drop me a line and give me the date, power output used, antenna used, stations heard, etc. As is usual with projects of this kind, we tend to be enthusiastic about it while the action is there, but a little remiss when it comes to looking back through the log book and putting pen to paper. An appeal on the VK3 and VK5 Divisional broadcasts yielded only one written report, so please sharpen up the pencils and send in your report, plus any comments, good or bad, that you have about the flights. After all, the Amateurs of Australia, through the Institute, are paying for the Australis project and they should be making the best use of the balloon flights and of the satellite to follow.

It was particularly pleasing on the 120K flight, to hear Eddie VK1VP in Canberra and John VK2ZHM at Coolamberrah, coming through the translator. The sort of distances covered in that flight give some idea of the coverage which will be possible with the A-O-B satellite, when VK-JA contacts should become commonplace on v.h.f.

The co-operation given to the Australis balloon project by Mr. John Hillier and his team at the balloon launching station at Mildura deserves special mention. The Australis translator was flown on a space, weight and power-available basis. While it was originally planned that there would be only one translator flight in the March-April series of balloon launches, George VK3YDB, by going to Mildura and talking with the HIBAL people, was able to arrange that the package flew on four, rather than one, flight. The active assistance given by John Hillier and his team in arranging the flights is greatly appreciated by the W.I.A.-Australis group.

(Continued on Page 27)

\* Chairman, Project Australis, 13 Neston Dr., Ringwood, Vic., 3134.

# KEY SECTION

During the 1960s an active element of Institute affairs was a group known as the Key Section. It appears to have dropped into limbo (with so many other things) in the early 60s, and did not reappear after the war.

The 1971 Federal Convention in Brisbane agreed to revive the Key Section, and the rules for its operation which were accepted were these—

1. That the Key Section be open to all members who have worked at least 50 different stations by two-way radio contact using A1 or A2 mode. To qualify as a contact significant text should be exchanged, say, 30 words apart from RST, operations during contacts are excluded.

2. That the Federal President's Cup, awarded to the Key Section of the W.I.A. in 1930, be revived and mounted and awarded annually with inscription to the member of the section who claims the greatest number of contacts using A1 or A2 mode in that year. No member may hold the cup for more than two successive years.

3. That the W.I.A. make available to overseas Amateurs a certificate or other token for working 20 or more members of the Key Section of the W.I.A.

4. That the W.I.A., through its Key Section, make available certificates of proficiency to members of the Section for successfully receiving and sending using A1 or A2 mode at speeds of 15, 30, 35 and 30 plus words per minute.

5. That the Federal Contest Manager be approached to alter the rules of W.I.A. contests to remove the bias against the use of A1 in contests because of the lower scoring rates which can be achieved using this mode under contest conditions in Australia, such as by offering a multiplying factor for all contacts using A1 or A2 mode.

6. That every method be used to introduce more A1 or A2 to the v.h.f. bands even to the extent of making operation of v.h.f. part of the requirement for some of the awards associated with the Key Section.

7. That the Key Section be managed by a group consisting of an officer appointed by the Federal Executive and a nominee of each Divisional Council.

8. The nominee of Federal Executive will act as nominal head of the group and report the activities of the Key Section to the Divisional Council.

9. The Divisional nominees will be appointed by Divisional Councils and will be known as Divisional Co-ordinators. Appointment will normally be for a period of three years.

10. In the event of a Divisional Co-ordinator resigning, or being replaced as nominee by the Divisional Council, a new nominee will be appointed by the Divisional Council, the tenure dating from the time of the new appointment.

11. The Divisional Co-ordinator may call upon the services of not more than three other persons, whose appointment must be ratified by the Divisional Council, to assist him.

The Federal Executive have appointed Deano Blackman, VK3TX, as Key Section Manager. The appointment of Divisional Co-ordinators, which is the next task in setting up the Section, is in hand.

# ANNOUNCING A SPECIAL CALL AND PREFIX

KC9KC will be heard on all bands for the period 1st July, 1971, through to 31st July, 1971. Members of the Mobile Amateur Radio Awards Club Inc. (M.A.R.A.C.) and the Independent County Hunter Nets meeting in Kansas City through these dates will man the station around the clock.

KC9KC will be on 10, 15, 20 and 30 metres, beginning when the band opens in Kansas City around 1300 GMT until the band closes late in the evening. Activity on 40 and 80 metres will probably begin around 2200 hours GMT until 1300 GMT the following day. However activity will generally be on any band at any time that hand is open.

Activity is planned around the following frequencies—

	CW	Phone(1)	Phone 2
80 Metres	3590	3680	3610
40 "	7050	7205	7260
20 "	14250	14205	14285
15 "	21050	21280	21360
10 "	28050	28000	

Notes: (1) Several times each hour operator will announce and listen 5 or 10 KHz. below the bottom of the U.S. phone band for DX stations.

(2) If "pile-up" develop, operator may listen off his transmitting frequency.

Log all contacts in GMT.

For special QSL, send SASE or two IRCs to (or via W0 QSL Bureau):

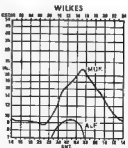
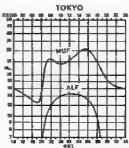
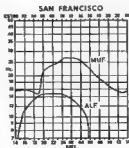
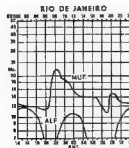
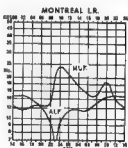
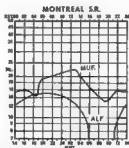
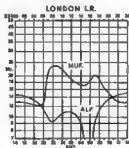
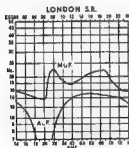
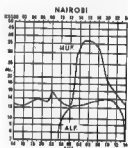
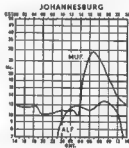
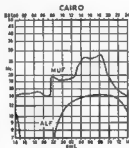
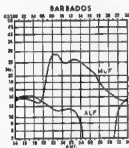
KC9KC or WA0WOB QSL Manager

P. Box 785, Shawnee Mission, Kansas,

66201, U.S.A.

# PREDICTION CHARTS FOR JUNE 1971

(Prediction Charts by courtesy of Ionospheric Prediction Service)



# May Tak to You About the 35th Federal Convention in Brisbane

In last month's "A.R." the "Wind of Change" was mentioned as if it had been something sudden. It is and yet it isn't. Zephyr breezes have blown for some little while. They have now increased to the point where their influence is doing much to improve the exchange of information in an efficient way at a meeting such as the Convention. Every Divisional Councillor and the many observers at the Convention all commented on this. Your Federal President is largely responsible for this. His overseas trips helped, of course, enormously. The main objective for all of us is communication effective communication. If this can be achieved more positively with less formality, so much the better. The pendulum could swing too far the other way. This is recognised. But we are dealing with persons, not faceless monsters or remote bodies out of reach and out of touch.

Which brings me back to people. Recognition of problems and genuine attempts to resolve them. This is what the Convention is all about. This is what the Delegates desire. Your problems are not too many. I.T.U. and I.A.R.U. seem remote. Not your problems you might say. How wrong could you be? You want I.A. to be there to help you in many ways. In the beginning to help you to learn the fundamentals of electronics, to absorb and use the Morse Code, and to put you in touch with cheap gear and components. Later on the emphasis shifts as you yourself develop expanding interests. You are bedged about by Regulations and many may seem too many. In 1910 the W.L.A. began. Not only for social contact. Not only to present a united front. But also the sharing of benefits which only a large group can command. No, I will not enlarge on this here except to say that the W.L.A. interest in I.A.R.U. is not misplaced. Without the united front—world wide—we would definitely not possess the funds we have today. Pressures by commerce, by governmental agencies and by many other services would have seen to that.

So, at the Convention, I.A.R.U. and I.T.U. matters received much attention because of Michael Owen, VK3KI, and Peter Williams, VK3JZ, had returned a few days beforehand from the I.A.R.U. Region III Association Conference in Tokyo and the I.T.U. Space Conference is scheduled for July in Geneva. Yes, plans had been laid. Keep your fingers crossed; we might need what we have. We could even hope to gain a little ground. For I.A.R.U. affairs, David Rankin, VK3QV, was appointed to be our Liaison Officer.

Equally, at this Convention, the financial side of W.L.A. affairs got a very good airing. The theme was how to do more at less cost. Facts of life have to be faced however. There was absolutely no question of how to squeeze more money out of members. In fact the contrary applied. Can we do anything more for members within our budget and, if so, what and how? As a newcomer to the Australian scene I was impressed by the massive amount of thought devoted to financial matters. I assure you it was not put on for my benefit. I am too old a hand to be hoodwinked into a belief that this was mere window-dressing.

The proposed computerisation (horrible word!) programme took two full pages of my notes. It stands to reason that, if the thing is done properly, savings can accrue. The most fantastic depth of detail unfolded before Delegates' eyes. Even down to such minutiae as how to preserve the confidential nature of information to be sought from members. How to get essential data and the practical steps required to process it were all covered as well as the relative importance of the end result. The computer can churn out, in seconds, any collection of detail which may be required. Not only print-outs of names, call signs and addresses for the call book, for magazine wrappers and unprintable other needs—transient and permanent—subscriptions and their apportionment, but, furthermore, bulk statistics of one kind or another which Federal Executive must have in their endeavours to convince disbelieving authorities of the correctness of their submissions. So, if you have to send your subscription to Melbourne next year or, if you are asked for any details you think may be important, don't worry. The whole thing is under the most rigid Divisional control. The Federal boys will not run away with the loot or misuse it.

Various technical affairs also took up a lot of time. Interference against us and by us and how best to achieve satisfactory results. After all, we pay four equivalent to others but receive different treatment. The U.S.A. phone operators petitioning FCC for a further 80 KHz. downward of band allocations and how we can most effectively display our opposition. Project Australia and the dearth of details for you received much comment on how to put this right. The back-room group are doing a splendid job all right, but for goodness sake tell us. Our money is involved apart from anything else, a plan was devised and John Batistich, VK3OF, is the corner-stone. Now the V.H.F. Groups in Divisions will have a chance to play with the light-tested package. Dr. Denise Blackman's proposed Key Section got off the ground. Traffic nets regularisation (i.e. vox), operators' identification "at the beginning and end of transmission—what is a 'transmission'?" how long, break-in—7050 KHz. was designated as a calling frequency as, for example, calling for aid on safari or using it for speed-making and then QSYing elsewhere—people could leave their receivers running on this frequency—and so on. Space does not allow me to go into detail I fear.

"So You Want to Become an Amateur" booklet is now in print and a very good one it is too. The only error detected so far is the fee payable when applying to sit for the exam, should, of course, be £1.00 but there are rumblings about raising it. The New Call Book should be out by the time you read this. Much criticism about the delay, which, incidentally was not our fault. How to deal with "A.R." and Divisional Bulletins—how can we economise without lowering standards?

Is that all? Do not be deluded. The discussions on the "Novice" licensing report (received only a week beforehand by the way) from Mr. Rex Black's (VK3YA) Committee got through seven pages of my notes. What

do you mean by "Novice" licensing? Like the JAs on 15 metres? No, but definitely not. The report was too good to set it on one side but much more thought and discussion is required before we can go further. Divisions have it. Why not ask about it? As one Delegate aptly remarked, "It's a large thing with few knobs to hold on to." General organisation and the efficient administration of W.L.A. affairs received attention in the light of the impending change-over to the new Federal Constitution after the W.L.A. Company Memorandum and Articles of Association have been signed, sealed and delivered. All this was, of course, tied in with the financial arrangements, "A.R." policy, and the role of the new Secretary-Manager.

Those who were in the 20 years of age group in 1910 would now be in their eighties. With the years, most of the pioneers will be passing on. The Convention again devoted time to ways and means to summarise and preserve items of historical interest. The onus has been placed on Divisions to examine this aspect, by looking up the names of local libraries and museums. Let us gather together everything we can before it is too late.

Another item was the change-over of the Federal Executive from VK3 to VK4. What a magnificent job they did on this over the past six years and we look forward to another good job expected next year. We have Peter Brown, VK3JF, is mixed up with it. Symptomatic of the times, by the way, were the very reduced numbers of agenda items about contests and awards rules. A good thing this, so please don't brow up a load of new alterations! Let the people in VK4 get the best of the thing. Geoff Wilson, VK3AK, naturally got a commendation on Federal Awards, especially for his excellent handling of the Cook Bi-Centenary Award. Ken Pincot, VK3FV, was commended for his devoted Life Membership and had his badge bestowed upon him at a moving little ceremony, and Alf Chandler, VK3LC, was commended on his part of running the Publications Department which will henceforth lend up on my table.

I know I have had to leave out a lot, e.g. repeated and heeded requests for publications policies, submissions about multiple-choice examination papers and operating procedures, etc. Don Wainwright, VK3JH, will vouch for this. He sat in as an "observer" for the VK3 Delegate. This was another new departure. The local Division provided "observers" for the far-away Delegates and this innovation was much appreciated not only by the Delegates but also by the "observers" themselves. The point is well taken, with innovation and modernisation, that we must keep the best of what we have however.

The venue of the next Convention is to be Melbourne for several valid reasons.

I started off this article about the I.T.U. and I'll end about it also. Tom Clarkson, ZL3AZ, will be attending the big July Conference in Geneva as an observer on our behalf. As somebody said it would be difficult to find a better qualified person anywhere in the Region III which encompasses the whole area roughly from India to the mid-Pacific. The Delegate to this Conference are officials of governments. Amateur Radio is only a small part of the whole and must be content with observers. We've done our part with our government. Have you done your part with your Division? T2 VK3CIT.



Photograph of Federal Executive Delegates at the Brisbane Convention of the W.L.A., held over Easter. Right to left: David H. Rankin, VK3QV (Sec. Mtn.), Peter Williams, VK3JZ (President); Peter B. Dodd VK3CIT (Sec. W.L.A.), Ken E. Pincot, VK3FV (Editor "A.R.").

## Wireless Institute of Australia Victorian Division A.O.C.P. THEORY CLASS

commences  
**MONDAY, 16th AUG., 1971**

Theory is held on Monday evenings from 8 to 10 p.m.

Persons desirous of being enrolled should communicate with Secretary, W.I.A., Victorian Division, P.O. Box 36, East Melbourne, Vic., 3002.

(Phone 41-3535, 10 a.m. to 3 p.m.)

# Adjustment of Output and Loading, SSB Transmitters

HEATHKIT SB-610 MONITORSCOPE AND HEATHKIT HN-31 ANTENNA

It is well known that a cathode ray oscilloscope is a valuable aid in checking the operation of a transmitter. The usual CRO is primarily a general purpose instrument for the laboratory or electronics workshop and is not always convenient to use in the Amateur shack on a permanent monitoring basis. The **Heathkit SB-610 Monitorscope** fills the gap, as it is designed to be connected into a 50-72 ohm antenna feeder line. Includes a built-in two-tone audio oscillator, is compact in size, and styled to harmonise with the equipment.

Adjustment of an output pi network of a PA stage requires care in order to obtain the highest possible RF voltage peaks without "flat topping". Some manufacturers give approximate settings of the loading control for each band, which with plate tuning resonance, is intended to assist the operator to reach this objective.

Installation of a Monitorscope enables a "picture" of the PA RF output to be observed, and when tuning up with the aid of the two-tone oscillator coupled to the transmitter microphone input, a regular pattern can be obtained to show the effect of tuning adjustments. It is relatively easy to arrive at adjustments which result in maximum deflection before "flat-topping" occurs.

The SB-610 also has provision for coupling to a receiver to enable visual monitoring of received signals. In addition, the instrument, with its H sweep and V amp., is useful for other CRO testing applications in the Amateur shack. A comprehensive instruction manual describes the various features and installation procedure, and operating instructions include representative screen patterns showing examples of correct and incorrect tuning not only for the SSB mode, but for AM, also keying patterns for CW, RTTY adjustments, etc.

It is recommended that tuning up be carried out with the transmitter output connected to a non-inductive dummy load. The Heathkit HN-31 Antenna is designed for this purpose.

## Brief Details

**SB-610**, applicable over the range 160 to 8 metres, has standard UHF co-ax. sockets for ready connection into co-ax. feed line, 3" mu-metal shielded CRT, power requirement 240 V. AC 50 c/s. Size: 6" h. x 10" w. x 11" d.

**HN-31** provides 50 ohm non-inductive load with SWR less than 1.5:1 for frequencies from 1.5 to 300 MHz. Co-ax. fitting to transmitter line. Phono jack for relative power measurements. Oil coolant (capacity 1 gallon—oil not included) permits power up to 1 kw.

ENQUIRIES ARE INVITED FOR ANY MODEL OF THE HEATHKIT RANGE OF AMATEUR EQUIPMENT

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## GELOSO T25 DYNAMIC MIKES

With push-to-talk switch. Twelve at—

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## GELOSO TRANSISTOR P.A. AMP.

30 watts, mains operated. Two mike inputs. Handy general purpose amplifier. Twenty only at—

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Five bands: 80, 40, 20, 15 and 10 mc. Tubes: 6J5, 6AU6, 6L6G. Complete with dial scale. Five only at—

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## EDDYSTONE U.H.F. RECEIVER

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### VOICE CONTROL

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## Page 21



## Amateur Radio, June, 1971

Sub-Editor ERIC JAMIESON, VKLP  
Forreston, South Australia, 5253.  
Closing date for copy 30th of month.  
All Times in E.S.T.

# AMATEUR BAND BEACONS

VK3 83.544 VK3GR, Antaresholm.  
VK3 144.380 VK3VY, Vermilion.  
VK4 144.380 VK4VY, 107m. w. of Brisbane.  
VK3 83.000 VK3VY, Mt. Lofy.  
144.800 VK3VY, Mt. Lofy.  
VK3 83.000 VK3VY, Tuart Hill.  
83.000 VK3VY, Carnarvon.  
144.800 VK3VY, Mt. Barker.  
144.310 VK3VY, Tuart Hill.  
433.000 VK3VY (on by arrangement).  
VK3 144.800 VK3VY, Devonport.  
VK3 144.800 VK3VY, Christmas Island.  
VL3 144.800 VL3VY, Wellington.  
VL3 148.000 VL3VY, Christchurch.  
ZL3 81.000 ZL3VY, Japan.  
W 30.200 W3KQ, I.R.A.  
HL 30.100 HL3VY, South Korea.  
ZE 50.100 ZK1AA, Cook Island.  
ZK50 ZK50Q, Newell.

The Cook Island beacon is included this month although it has been around for some time. Doug VK3KIK in Darwin reports hearing it on 4th April with signals 840. The Hawaii beacon is being reported to operate nominally around 80.100, but reports indicate the frequency varies as high as 0.107. Doug has been having reports in Darwin with varying signal strengths, rising to 869 on 28th April at 1315 hours. It has also been heard by Ross VK4RO and David VK3AU. It is rather frustrating signal, however, as Doug reports that if you hear the beacon and dial 433.610 in Hawaii, after eight rings or so you are prone both to see and hear it. In this state you can then work yourself! As Doug says, "Just book your trunk call to K3H and you are prone both to see and hear it. In this state I wouldn't be either! To make matters even worse, it appears there is very little reliable c.w. activity in K3H, with KH6RU as the main signal, but beyond that I don't know whether he ever listens on 33 MHz.

Further notes on the Darwin scene are that six more reports across the beam before long on 33.500. (This is very pleasing information and further details are awaited—SLP.) Good signals to Bob C3L many times this month for his 33.500 beam. It seems to be a pipeline that way! Seems as though it is double hop F3 at K3H with C3L on the first hop. HL4WV in Borneo seems to be coming in better in Darwin, along with any number of JAA, with signals being as strong as ever heard on YE. The YE starts about 3900 and goes to 3600, and is like this four nights out of five, with all districts except JA7 and JAA. Doug works quite a number on c.w. plenty on s.a.b., but this mode still in the minority as yet in JA. Time is short with Doug for continuing much work with MS signals to David VK3AU at Tannan Creek but reports the improvement in signals since installing half inch foam bellows cable to the beam, which has a loss of 1.8 dB per 100 feet at 1.8 GHz!

# ACTIVITY IN CANBERRA

VK1DA reports there are about seven stations operational on the non-net sections of 32 MHz., and has been able to use the channel of 83.533 MHz., but operation is spasmodic. On 144 MHz. there are about five stations with reasonable equipment, but only regular contacts appear to be the skeds between Eddie VK3VP and Alec VK3AAK on 144.000 MHz. Ab/c/cw on 144 MHz. stations operate on Channel 8 f.m. with regularity, plenty not so regular. Charlie VK3IC is working Sydney stations on Channel B with fair success most nights. Keith VK3AA is running a net on Channel 8A at Young generally are good copy in Canberra. Graeme VK3CG listens and calls on a.m. on c.w. and s.a.b. but reports no regular contacts. VK1, and the boys are beginning to wonder if anybody in Sydney operates in the lower parts of their bands.

Andrew reports it seems unlikely Canberra will have a repeater for the f.m. channels because it would not significantly improve the coverage of the stations. The repeater would be a little help in increasing the coverage between mobiles in his area of the State. The locals therefore are more favourably oriented towards a beacon (excellent news—SLP) and present plans are to operate on 144.475 with low output, solid state, turnstile or dipole antenna, 5 seconds on, 5 seconds off, then 5 seconds of call sign in c.w., on an elevation a little above Canberra.

Finally, it is interesting to note the art of home building still comes to the fore in Canberra where at the recent Convention a competition for home-brew gear was won by Eddie VK3VP with a line up of varactor triplers and filters (144 MHz. input, 1200 MHz. output), and some 100 MHz. Second Harmonic was Neil VK3IZT with a 1200 MHz. converter and home-brew dish antenna. There's a two-one-one transmission made by Graeme VK3CG with 55 and 144 MHz. transmitters in the same unit with 6/40 500 watts each.

Brian VK3BB/4 writes from Atherton in North Queensland to say the paragraph in April "A.R." was inaccurate in stating he worked HL4WV along with VK6E, SKK and 8AU. He has not been active on 6 metres since leaving New Guinea and is now in Australia. Currently he is using 144 f.m., but the main trouble seems to be his isolation v.h.f.-wise. However, his work was increased at one or two points on the 144-400 edge of the Tablelands with a view to entering the Qld. V.h.f./U.h.f. Contest in May, and is constructing a sly-beam for the purpose. Brian is hoping to have some reasonable contacts into Townsville (130 miles from the best local high spot), but so far 146 signals from there are very weak.

# RTTY IN VK3

Signals a little different from the usual have been heard on 144 MHz. in VK3 for awhile now, and were finally tracked down to being r.t.t.y. being by John VK3JE at Pokoraka, north of Adelaide. John would be pleased to answer any queries from anyone regarding v.h.f. r.t.t.y. teletype, equipment, etc. To assist in this and in the hope of fostering interest, with eyes across the border to other areas, write to John E. Dunkley, 9 Elva Ave., Pokoraka, S.A., 5006.

# WFF RTTY NET

Further to the above, John has given a lot of thought to the establishment of an r.t.t.y. net and after discussion with other lenders has the following plan: Also require ship keying (a.s.f.k.) as this is more suited to v.h.f. operation, and facilitates auto-start, etc., and receives a number of other advantages. This f.k. as used on the lower bands. He recommends 144.800 MHz. as the net frequency, being located in some of the upper areas of the 3 metre band, being below the 433 MHz. band and is free of other nets and beacons. (There has been such a net on 144.840 MHz. in VK3 for some two years or more—E.S.D.)

# SEASON STATION

A little more news on this interesting phase of Amateur Radio. Wally VK3ZWW has been successful in establishing a net on 433 MHz. and VK3ZJW via MS on 30th and 30th April at about 0615. Signals were considered good when only random material were being used, and the contacts have been good enough to record the efforts on tape. So that makes two States for Wally now by that mode. Also in on the act was David VK3ZMO who heard Rod on 30th April. The story leading up to David's efforts arose from a comment following publication of the Contest announced last month by VK3. When mention was made that the stations with elaborate equipment would get anywhere. Challenged to overturn his own gear, David set about improving his receiving gear—the result—VK3ZJW. So one never knows just what can be accomplished until you try; good luck David, you might join the ranks of

those making such contacts. Wally reports that around 0600 to 0700 is the best time, particularly for random scatter contacts. He would be pleased to hear from anyone who might give it a go, as he is now on the path to attempting worked-all States via W3. Second Harmonic contacts with W3WV reveals there have been three known openings to JA during April, and stations were worked on two of these. He also has a tape recording of a contact received from HW1V1 on 30th April on 17th April on 50.100 between 1315 and 1345 hours, and the same station was heard on 18th April. During 1985, Wally was told JAXIV had worked an LU3 on 18th April, but no further news of this at present.

# 576 MHz. NEWS

Bob VK3AOT stirred up some activity in VZ3 in the early part of the year. Over Easter he worked Dennis VK3BDA at home at Mt. Waverley from Mt. Cowley, distance 83 km. signals 3 s plus; this just being a new VK3 record. Saturday and Sunday were spent in the Grampians on Mt. William. The path to Melbourne was a poor one, signals to VK3BDA 144.800 MHz. on 20th April, and 144.800 MHz. on 21st April. Two-way contact was made on 576 MHz. 8 x 4 both ways, 143 miles. On Sunday morning, 22nd April, Bob's signals to Dennis 840.30 miles south of Melbourne, and was received at 80, giving 87 in return. Distance 147.3 miles, a record. The previous VK3 record was 144.800 MHz. on 20th April, and 144.800 MHz. on 21st April. This is a revival of interest in 576 MHz. (John VK3QZ, holder of the present Australian record on 670 is waiting for a contact on 576 MHz.)

Further news from Bob on the VK3 scene shows that the last of the series of field days for the season held during Easter attracted 11 stations into the 433 MHz. band, and the longest contact was on 2 metres over 340 miles. It is good to see that a series of field days can be supported to wit, it is difficult to get many stations into the field in VK3 on one day a year!

On 1st May, elusive VK3 station, VK3ZEO in Deniliquin, was seen trying 433 with Ian VK3ZDW, but so far no two-way QSO has been achieved. This may be a contact worth looking into by the 433 operators in VK3, giving them another State.

Continuing, Bob reports excellent 3 metre contacts on 30th April, when stations from Mt. Gambier to Mt. Melbourne, and giving some of the lower powered Melbourne boys their first VK3 contacts. Mt. Gambier signals were also heard in Wangaratta and Deniliquin. On Monday night, the Melbourne Night Owls Club members had to contend with a very strong signal from the 3 metre beacon on Mt. Lofy, at 89, every one in Adelaide having gone to bed! VK3VE at Albany at the same time was 51, making it the 43th observed station it had been heard in Melbourne for the season. The excellent conditions extended themselves to 433 MHz. Colin VK3DK did Mt. Gambier hear contacts with VK3ZDW, VK3ZBE and VK3YDI. Also noted that Ron VK3IAK worked Kevin VK3AIF on 18th and 19th April.

As predicted in these notes awhile ago, this autumn was a time to keep a good ear on 83 MHz., and the period around Easter and the following months. A signal was heard on a telephone call from John VK4ZTB in Brisbane gave me the first hint of something to come. The following day a good signal was being heard in that city from Japan for several days, seven hours, and considered the best openings since 1958. John also mentioned in his phone call that Bob VK3VY was in the area, but this time nothing eventuated in VK3. Many thanks for your interest John, it was worth the effort.

In mind the privately sponsored V.h.f./U.h.f. Contest by David VK3AU to be held in July and details of which appeared in the issue.

A new station is operating from Casey Base in Antarctica with call sign VK3PF and Phil VK3VY operating on 33.640 MHz. No other details available at this time.

That's all the news for this month. Closing with this thought, "Someone has defined courtesy as the form of polite behaviour practised by civilized people when they have time." ZL, Eric, VK3LF. The Voice in the Rills.

# SOUTH EAST RADIO GROUP OF S.A.

# ANNUAL CONVENTION

will be held over the week-end

12th and 13th June, 1971

at MT. GAMBIER

Events will include 80 and 2 metre fox hunt, 2 metre relay, and sniffer hunts, scrambles plus other novelties.

Hotel and motel accommodation can be arranged if it is required, with a deposit of 50 shillings and a refundable 50 shillings. Convention reg. 85, includes all meals except cabaret Saturday evening.

All correspondence regarding registration to South East Radio Group, P.O. Box 1183, Mt. Gambier, S.A., 5206.

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# EDDYSTONE

CERAMIC MICRODENSERS ON 1-5/16" END-PLATE

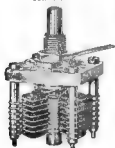
Cat. No. 583

## CAPACITOR CATALOGUE

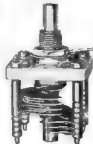


A comprehensive range of variable capacitors, well designed electrically and mechanically, and intended to stand up to continuous usage under all reasonable conditions. The types include single-section, split-ator, butterfly and differential capacitors.

Cat. No. 584



Cat. No. 583



Cat. No. 817

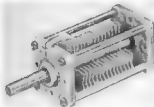


### TRANSMITTING VARIABLE CONDENSERS

Cat. No.	Type	Capacitance (pF.)		Proof Voltage	Air Gap (ins.)	No. of Vanes		Price
		Min.	Max.			Rotor	Stator	
815	Single Section	7.5	87	1,700	0.048	7	8	\$7.90
816	Single Section	9	102	1,800	0.054	10	9	\$8.16
817	Single Section	10	270	1,100	0.054	14	13	\$8.48

### HIGH STABILITY TYPE

This pattern, Cat. No. 726, has double end-plates, 1-5/16 in. square, and double bearings, making it particularly suitable for high stability oscillator applications. Single section type, silver-plated finish. Max. Capacity: 80 pF.; Min. Capacity: 8 pF.; Air Gap: 0.03-in.; Proof Voltage: 1200. Price \$7.81.



SALES TAX NOT INCLUDED

### MINIATURE MICRODENSERS

Particularly suitable for VHF applications and where space is restricted. Robust construction. Two-hole fitting, using parts supplied.

Cat. No.	Type	Capacitance (pF.)		Proof Voltage	Air Gap (ins.)	No. of Vanes		Price
		Min.	Max.			Rotor	Stator	
551	Butterfly	4.5* 2.8†	28.5 14.5	300	0.01	10*	9*	\$3.73
552	180 deg. Split-Stator	3.8* 2.0†	21.5 11.5	500	0.01	4*	4*	\$3.83
553	Single Section	3.5	54	580	0.01	10	8	\$3.28

\* Per Section.

† Series Gap.

AVAILABLE from . . .

**R.H. Cunningham**  
PTY. LTD.

VIC.: 608 COLLINS STREET, MELBOURNE, 3000.  
N.S.W.: 64 ALFRED STREET, MILSONS POINT, 2061.  
QLD.: L. E. BOUGHEN & CO., 30 GRIMES STREET, AUCHENFLOWER, 4088.  
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Phone 70-8087  
Phone 49-4918

(All times in GMT)

The most interesting development in the past weeks has been the upsurge of activity on 40 metres, and according to George ZLAFZ, SW also. Maybe it's because SW has deteriorated and sent the DX down to the lower bands, or that the lower frequencies have improved. Regardless of the reason, the result is that much really good DX can be heard and worked on these two bands.

George ZIAFZ reports a steep decline in the sunspot numbers, and lists the following figures: March 1968 the figure was 108, March 1970 83, March 1971 76 was the predicted count, whilst figures for next March are estimated at 48, for 1973 the estimation is 33, 1974 should be 20, going down to 10 the following year.

ZLSAX is occasionally active from the EL Antarcctic using 14020 at the week-ends. His operating times are dependent on official duties, but he has been noted at 8300z.

word that Alex will be going to Rodriguez in June, but to date no further information is available. Secondly, it appears that Alex wants QSLs for contacts made with the VK boys, and

John VKIKO asks me to make it known that if any VK wants the 1B7DA QSL, forward plus a stamped addressed envelope to him, John de Cure, 10 Portland Ct., Fulham, S.A. and the card will be sent to you when received from Alex. Should you want to send it direct, the address is Alex Mootoo, 1B7DA, 28 Brown, Seaward Ave., Vaco, Mauritius.

The following comes from AIN VKILC who passes on this information received from KKKK-Larry VKSNP, who is ex-KHXP, has left Townsville for Melissae Reef and will be operating from there for some time. The operation has been approved by the A.N.Z.L. as a new course.

DLTF will leave Berlin on May 34 to operate from an hotel in Albania using the call sign ZAEKPS. He will operate until June 7 with a 3 element beam using the following frequencies; c/w transmit 16005 and 21005, receive 14050 and 21000. Transceive on 20000. On a.s.b. he will transmit on 10105 and 21340. Receiving on 14330 and 21300. He may transmit also on 14105.

ZM7AG is on almost daily for Ws using 14017, and for others on 14180. Usually comes on at 0400s, remaining on for an hour and sometimes much longer. His name is Jim and he is a member of the school. It is possible there will be some time. (Further to Alf's note, there is a memo in Geoff Waite's bulletin of Mar. 17 reporting that the International DX Assn. was sending gear to a school teacher at the school. If this is the case, then the QSLs will go to that body. Don Sub-Ed.)

Finally Alf reports that VR5DK is due on from mid April for an unknown time, PR2TUZ will be active for two months from Mar. 14, and will be active from Australia for the next two months or so, and VS8HM is a newbie on the Maldives.

In passing, John mentions that VETWY has been having trouble getting QSLs from rare VK stations in the VK3 and VK5 call areas. QSLs have been sent to managers and directed to the stations concerned to no avail. Personally, I find this hard to understand. I have never missed out on a card from the VK areas and it is almost all my hobby. I have never. In fact I have found the VK3 boys most courteous and helpful, and I suggest the VETWY has tried the wrong ones.

Clipperton Is. has again emerged as a strong possibility, with FGXT hoping to take KWM3 and Iribander there in the spring, and F9QQ hoping to make it this month (April I prefer to wait and see, as this one has been the basis of far too many rumors).

JY has been in the news sheets far more than any other country over the past twelve months and it is now reported that King Hussein JYI is often in the Arabian net with STBA, SUIMA, YKIAA, etc., on 14300 a.s.f. at 0430z. JYI/B skeds WASHUP 21320 on Sa and Sundays at 1000z, whilst JY2 Prince Moosa is often on 14300 a.s.f. on Tuesdays.

Finland Postal Authorities have now stated that all operation from Market Reef must use OH9 prefix, and the word is that the country has been deleted from the DXCC list.

Still a lot of activity from the VP producers  
VP2ED on regularly from Anguilla, QSL to  
WB2ZMK VP2ED from the same location was  
May 1 has WASVOL as manager; VP2KY was  
due to go QRT from March 8, and all VP2  
has been operating on 20000 of 14.0 and his  
cards should go direct to Box 130, St. Lucia  
Also active from there is VP2LT VP3JA was  
the call used by the Was who went to Turin  
and Calico during March 27 contest week-end  
QSL manager for the operation is K6DZ  
New Orleans, 6042 Sapphire Dr. Jacksonville  
Fla. 32209

The WASUNK Golden Microphone of the Month award for QSL manager of the month of February was awarded to KH6GLU, Ed Young, who is well known for his handling of the Pacific and DX Net, and the QSL chasers connected with it.

The special prefixes FP, PV, FW and FY were made available to PY stations during the WPX contest on the week-end of March 7-8. QSLs for any station using one of these prefixes should go to their PY call.

Another special station was WC45FF, which was operating during February of this year at the South Florida Fair. The QSLs should go to Box 461, Lake North, Florida, 33469.

Kevin ZK1BM has been in the Pacific Net on occasions, and all his QSLs should go to WTVR who will also handle cards for ZK1C after 11/3/71.

With reference to the QSL managers living in the States, I get quite a lot of letters asking for the QTH of these chaps. Unfortunately, I do not have an upto date W call book here and I am unable to help. My call book is about 16 years old, and as well as being obsolete in the usual sense of the word, it does not carry the zip codes without which letters are often returned. As mentioned earlier, I have the DX News sheets from Geoff Watts covering the last two years and can pass on any information from these. But U.S.A. calls, I can

CRSAK was due to be activated by a J over the WPX week-end and the following two days. The operator was JAIKAE, Jim Suzuki, 6-9-14 Kanamachi, Katsushika, Tokyo 123, Japan, to whom all QSLs should be sent.

The current operation from FM7WN which seems to be on all bands at any old time has DJEB as general QSL manager, whilst KICGQ will handle QSL for the American gang only. From San Andreas we have some QSL info, mostly the current K6RCK operation, which was WAAHF as manager, whilst the QSL for the operation over the last week in Jan are a little more complicated. K3CQV and W3UCW both operated as /K6K and their manager is W3DQ. The other two using the

Three more prefixes for the WPX week-end, HUNO was YS2CEN on 14 a.s.b. QSL to WA-2STDY. HW6KAW was a special operation by F6KAW. QSL to Radio Club DX divory, 8 Rue St. St. Just, Tour F 91 Ivry-sur-Seine, France. The IC prefix was due to be used on April 12 by IC1AA, SEZ and ZGY from S. Pietro Is. QSL to DXOTC, Box 143, Palermo Sicily, plus three INCA.

Further to the operation from Nayama Is. from Feb. 8 to 12 by W6KXD/KC4, it has been confirmed that the QSL chores will be handled by W4OHP.

Some stations currently operating from U.S. islands in the Pacific are KG8SL, QSL to WA-6AHP, and KG8SW, QSL to WYTWX, both in Saipan in the Marianas. Geoff Watts news-sheet lists KG8SW as having WYTWX as manager, and it is probably right. WYTWX is also in the Western Carolines. QSL to the operator is home call WF2DP. From Johnston Is., WB-6HQZ/KJ8 is active, manager being WB6HSD. WAIARF/K94 is listed in the Long Is. DX Ann. bulletin as being active from Swan Is. where he is now working. The operation is not a DX-pedition, merely a QSL to go to WA6HSD's work schedule. Normally QSLs go to WA6HSD.

MPMBEN is a permanent skeds go to  
MPMBEN and KMQQG on 1430U skeds via  
and KMQQG on 1430U skeds at 1330z on  
the long path to U.S.A. He is in the British Com-  
monwealth Net on 1335d daily at 1430z, and  
accepts skeds via his QSL manager GSIQF.  
SHMHM is shortly due to return home, but  
if you want a contact with him, try via his  
QSL manager KEZIF, he is often around 1430z  
or 2130z c.w. only. In the same direction,  
SHMOEA Chuck has been reported in the  
States on 1430U and 240 s.a.b. His address is  
Box 796, Kuching, Sarawak.

There has been recent activity from Comoro Is. during the French contest, **PHCY**, Box 438, Moroni; **PHCG**, Box 125, Moroni, and **PHCE**, Box 268, Moroni, being the main stations.

FRATEP/E from Europe, name Maxime, has a daily feed with JAOCUV/I, probably on 14190 at around 1300z, but reports from the States say his signal is very weak.

The IDI prefixes used over Mar. 19 to 21 are valid for Islands of the Air Award. Prefixes are also valid for the Islands of the Air Award. The Islands are situated in the Southern Adriatic Sea between YU and Italy and do not count as a separate country. The arrangement for the IDI operation is as follows: I will be the IDI operator, you send to IDUW, and another sends to IIBGJ, and another says either. So take your pick on this one. If you are not in a hurry and want to use the bureau, send them via the I.S.W.L. Bureau in England, or if you prefer, send them to me and I will take them on, as I have a regular despatch to that Bureau.

Recently 7TJLAW operated from the Camerons during an important contest. During his activity on 10 meters DX was reported to be very good. Many multipliers were made by many other rare DX stations who happened to be in the area. This is just another example of the chaotic conditions that exist when a mob of jealous incompetent operators who are quite incapable of operating a station do their utmost to prevent the other chap from doing his best. The DX chase is a very noisy operation or DX chasing either. Many of these idiots forget that an experienced operator can hear a signal that is not heard by the rest of the mob. I mean a c/w signal, and if they regularly listen around the bands it won't take long to identify the offenders, unless of course the trouble is caused by a station that is not in any action as far as I am concerned would be to blacklist him. This is a term which I have used, but with the pleasure of being ruined by a lot of selfish characters. The drastic action is the only answer. The bulk of the above comment is taken from the Long Beach News.

YOWU and YOWUJ, Sever and Maria Diaconu, now have a stateside QEL manager, WERTSE, R Tynar, 5 Chelmsford Dr, Wyandanch, NY 11798, U.S.A.

Finally, and to clarify any misunderstandings which may be floating around, I have resigned from the VK2 Division after having been a member of it since 1987. The reason is

personal, but as a result of this, it is only fair that I should come to write for this magazine, and the Editor has been notified accordingly. I have indicated, however, that I am prepared to remain on the job until a suitable replacement becomes available. I stress the word "suitable" because I am not a "jack-of-all-trades," and I feel that despite what the individual Divisions think about work on "A.R." being spread over the various States, the various Sub-Editors should be situated in the same State as the magazine. This would obviolate any unnecessary delays due to mail-handling, and also have the Sub-Editors in close contact with the general Editor. I am,

# Overseas Magazine Review

Compiled by Syd Clark, VK3AGC  
and R. L. Gunther, VK7RG

## FOREWORD

Relevant to the review published in the April "A.R." for Ham Radio, 1 Jan. 1971, in my haste to defend antenna couplers I overlooked something important in WB3QY's article, "Inexpensive SWR Indicator". I wish to comment on it here, because of some important principles involved.

In that article a primitive "SWR Meter" is supposedly obtained by a detector fed from a loop slipped around co-axial cable. The loop is run back and forth along the co-ax, supposedly to measure the distance between standing waves.

Unfortunately for this cunning idea, standing waves in a coaxial cable are confined to its inside surfaces. It is most dubious whether this can, as the author suggests, be reflected by a kind of leakage or induction from the surface of the braided-shield to be picked up by his loop.

Any such outer-surface a.s.w. would be a function of the antenna impedance, with the principal consequences of distortion of the antenna pattern, and of radiation from (and pick-up by) the transmission line. The cure is simple: use a suitable balun. This subject was discussed at length in 1968 issues of the "Australian EEB"—and so I certainly ought to have spotted the error sooner!

It is not sufficiently appreciated that antenna matching involves two variables: matching the line to the antenna (or conversely, and matching the antenna to the line). The latter is not terminated in its characteristic impedance it will develop standing waves. As W3J3 has pointed out in recent Amateur literature (e.g. EEB's April 1970 issue) the line will have relatively little consequence for v.s.w.r. less than 5:1 at frequencies less than 30 MHz. In terms of power loss, but they do complicate transmitter matching by presenting it with an indeterminate reactive load. Thus the usefulness of the antenna coupler becomes evident, which acts to filter harmonics even in an ideally matched system.

Aside from the over-rated role of a.s.w. at h.f., the fact still remains that a.s.w. readings from the antenna (or the bridge) using a.c. bridges can be misleading (as discussed widely during the past few years). In addition, optimum antenna-to-line matching depends on a decreasingly large number of difficult-to-control variables—as discussed most interestingly in the October 1970 issue of "Spectrum" IN-2, in the article "SWR 1:1, Fact or Fiction".

The answer to proper antenna matching is, of course, the use of suitable instrumentation, the use of the Antenna Bridge (EBS 1970, "A.R." 12/70), r.f. bridge with slotted line ("A.R." 10/70), or "Antennascope" type of invariable r.f. bridge (Gorr, "Radio Handbook", See also comments in "Ham Radio" of November 1970 with a very interesting exchange between a correspondent and an author on the real meaning of reflected power—VK7RG).

## AUSTRALIAN EEB

**December 1970—**  
FET Conversion of EECM's Heterodyne Frequency Meter, I. N. Kallian, VK1. Useful information of great interest to those without instruction books.

A C-D Ignition with Automatic Changer, T. Vierz, VK4. Sold to add zest to tired motor cars.

Commensurate Transmitter Loading, C. C. Drumeller, W3J3. If your transmitter does not load properly, this is for you.

## February 1971—

A Tachometer for Capacitor Discharge Ignition, VK3ZAR. More on "solid state" systems for motor vehicles.

A Nice Phase-Modulated Two Watt Tube Transmitter, L. Osborn. Small, neat and tidy.

A Sythe-Sense Tester, T. M. Palmer, VK2. This worried me for a while and then I realised that it would spell it Scythe. It seems that once again sharpening blades have keen properties.

The Use of Avalanche Diodes, VK7RG. An interesting discussion of modes and a means of checking unmarked units.

## BREAK-IN

**Jan.-Feb. 1971—**  
The Christchurch VHF Repeater. All valve job, neatly packaged.  
R.B.M. Two Metre MOSFET Converter. ZL3TAU tells how they made this a V.H.F. Group project.

Solid State Quick Check, ZL3YAT. Tells the user whether or not the translator function is okay or not. Naturally it also checks diodes. In or out of circuit, powered or unpowered.

## March 1971—

Direct Reading Capacitance Meter, ZL3ADE. Reprint from "E.R." Apr '70. Covers 8-10 pF and 0-1 uF, in six ranges with linear scale. Accuracy quoted as  $\pm 1\%$  plus or minus 5%.

Transistor Checking with an Ohmmeter, ZL3AHP. Identifies the types, silicon or germanium, NPN or PNP and checks which lead is which.

Teletypewriter Equipment Speed Control Data, ZL3ALW. How you can do something about getting your teletypewriter operating at the correct speeds.

## CO

**November 1970—**

Electronic Keyers—1970, W4MXX. Modern IC circuits of simple and lambic keyers for use in keying transmitters. A 2N3440 transistor is used in the keying stage to plus or minus 5%.

The LRD (Lightweight, Study, Discovers). An omnidirectional v.h.f./u.h.f. antenna.  
Review of Drake SSB-1 Receiver, by W3AEF. Described as "a versatile solid state job for operation with a.m., a.s.c., c.w., or r.t.t.y., or at selected 500 KHz. segments in the range 150 KHz. to 30 MHz."

A Simple D.C. Voltage Dropper, W3FEZ. Using a six-volt tap recorder from a 12 volt battery.

Evaluation of the Deetzel, Part 2, K3EBZ. The concluding article in a two-part series describing an every-day approach to understanding the "lightning bolt".

Improving the Elex 133 Transceiver, W3CWW. Some of these were sold in VK so there may be men who are interested. The power supply offers regulated 75V, 100V, h.t. The National NCX-A power supply is similar, but without the regulation.

## December 1970—

A Solid State Comm. Receiver, 117DJ. FET front using T183A, tunable 1.1. on 2.5 MHz, followed by mesh filter 1.1. on 350 KHz. Uses Command set for 1000 Hz. h.t.

An Inexpensive Utility Antenna for 80 Mx, W3SAI. Simple certainly!

A Digitally Divided Frequency Standard for Lab or Receiver, W7UJ. Using four Motorola 10A, this unit gives outputs on 1 MHz., 100, 50 or 25 KHz. and 5 KHz. Signals are stated to have readable error at least 100 MHz.

In Defence of CW, W3EO. Should be read by all who feel that it should be dropped as a requirement for Amateur status.

Keyed Solid State Oscillators, Di Ming Lee. Transistors at the heart of the resonator, for the drift are different and it can be minimised. Here's how!

An AZ-EL Antenna Mount for Satellite Tracking, W3AEF. Uses two R.C. rotators, one on each axis. The rotators are sold here by R. H. Cunningham & Co. under the brand name "Solitrol".

An FET RF Attenuator, W3EEY. A useful device to avoid receiver overload effects due to strong signals. One of the circuits in Fig. 2 checks a return leaving the 5 to 9 v. battery "up in the air".

Improving the Home-Bi-Rider Indicator, by VK3AGC. The meter of this voltage related supply keeps indications "on the beam".

## January 1971—

QSK with the Heath SB-Series Equipment, Rev. C. The receiver operation is not only desirable for high speed c.w. rag chewing, but is a must for fast, efficient traffic handling. Simple modifications enable such operation without sacrificing ease of operation in the a.s.b. mode.

F.M. KRSTIĆ. An introduction to the joys and problems of this operation is not only desirable for high speed c.w. rag chewing, but is a must for fast, efficient traffic handling. Simple modifications enable such operation without sacrificing ease of operation in the a.s.b. mode.

The Wave-Loop Triband Quad, VK3AOU. Operating principles and two element quad mounting details.

Sungate Cycle 20, Progress 1970, Prediction 1971, W3ASR. Enables you to decide the most profitable operating times and arrange, in advance, to be there.

**An Amal Diode Transistor Tester, W3EY.** This tester provides a simple rapid indication of resistance values so one can concentrate on the components being measured without the interruption of having to examine a meter scale every time a test connection is changed.

## February 1971—

An Introduction to VHF FM Sub-titled L.M. techniques for non-FMers, W3HPI/G. F.m. offers significant technical advantages over conventional a.m. and some over a.s.b. The author describes the merits of L.M. and the construction of two accessory devices to receive and transmit L.M. on the v.h.f. bands.

F.M. KRSTIĆ. Feature  
Calibrating FM Deviation, V3AQY. Describes the Bristol Z.M. method of calibration which is an absolute method of calibration.  
The Table Top Maxi Linear, W3KI. A 3CX1000A1 for 80, 40 and 20 metres.

## OEM—The Oriental Ham Magazine

**Nov.-Dec. 1970—**

This is a nice little magazine which is published in Tokyo and is usually filled with pictures and jottings about the goings on in Asia generally. This issue carries the news under the Govt. of Japan. It is likely to approve reciprocal licensing in the near future. No doubt this will boost her image. Also, Three Cards, Z3IAZF. Discusses the difficulties of getting cards from rare countries and methods of achieving the near impossible. Of course, if you were one of two or three Americans who were in Japan, you might feel the problem is yours in coping with requests.

The technical content is "The GARN" by G3R. The many amateurs know this antenna quite well as it allows all band operation with one antenna from a location of limited extent. Do VKs know that GARN is now VKSLV!

## January 1971—

Electronic Keyers, V3BAM describes a simple unit using a single transistor and about a dozen other components. Operation is from a 9 v. battery.

The balance of this issue is given over to stories of various happenings from here and there, mainly in the Orient.

## QNT

**November 1970—**

An Advanced General Coverage Amateur Receiver, W3BA. A very interesting specification for a receiver who has a lot of tubes they wish to use.

100-300 MHz. Broad Band Inverted Vee Antenna, W3P. Describes the details of how the system operates and shows how to construct a practical two band version of this effective antenna.

A V.F. for 80 Through 15 Metres, Di Ming Lee. Here is an idea article showing how to use varactor and PIN diodes to tune and switch a variable frequency.

A 2-500Z Grounded-Grid Amplifier for 80 MHz, W3GVF and W3HQP. Simple high power for owners of medium powered exciters.

A Station Control Unit for the Blind Amateur, W3P. First integrator circuit for the blind. W3H. It is handicapped. Amateur needs only 2x, 2x and antenna.

## December 1970

Conversion MOSFET Receiver, by W3ZJO. Those of you who are seeking a modern design should be interested in this one. Single conversion, MOSFET mixer with 9 MHz. IF and 2.5 MHz. local oscillator, uses standard transmitter components. A compact and sensitive receiver for 80 and 20 metres.

An Antenna Box for Amateur WHOG. Very useful for measurement of amplifier gain and other audio jobs.

Some Notes on the Design and Construction of a Broad-Band Linear Amplifier, W3LX and W3U7A. If you have a spare 3-1000Z doing nothing you can put it to work. There is a second version using a pair of 3-500Zs for 80 and 20 metres.

A Wide-spaced 35-ft.-element Tribander, W3FDY. Measuring 35 ft. 8 in. along the 20 m. reflector and 35 ft. 8 in. on the beam, this is quite a lot for an antenna raising party to handle.

A High Output VFO for a Beginner's Transmitter, W3AEK. Output is on 3.5-4 and 7-13 MHz including a 5v. amp. and broadband 1:1 transformer. Solid state.

Nightlighted Intense Sporadic-E Propagation, W3ELI and W3EDQ, Part 1. Causes and remedies. The result of observations made since the 1920s.







**TWO METRE F.M.**

*from* **YAESU**

# FT-2F All Solid State TRANSCEIVER

Up-to-date advanced semiconductor techniques. 25 silicon transistors, 16 diodes, 1 SCR, 2 ICs, 1 FET.

The YAESU FT-2F opens the door to noise-free, broadcast quality two meter FM operation. And thanks to repeater stations in operation around the country, the two metre band is no longer limited to line-of-sight communications.

The FT-2F Transceiver is a highly advanced, all solid-state unit complete with an automatic tone-burst signal, with an on-off switch, for repeater actuation. The FT-2F has channel capability of 12 simplex or duplex frequencies. Three channel frequencies are included in the purchase price of the FT-2F. (Sets imported by B.E.S. will have simplex Chs. 8 and duplex (repeaters) Chs. 1 and 4 with crystals installed and aligned — six crystals.)

Advanced circuit design protects the rig automatically from the damage of transistors caused by antenna trouble, or reverse connection of the power line.

Nothing could be simpler than the operation of the FT-2F. Just select your channel and begin push-to-talk conversation with fellow two metre enthusiasts. A simple meter on the front panel indicates battery condition and relative power output. The meter automatically reverts to 8 meter operation in the receive mode.

Portable or home-base operation can be achieved with the addition of the optional FP-2 power pack. This AC power pack provides regulated DC power for the transceiver and charging voltage for optional lead-proof re-chargeable colloidal type batteries. In addition, a high fidelity elliptical style speaker is built into the pack. The FT-2F of course has its own self-contained speaker for independent use.

In the event of a disaster causing AC power failure, the FP-2 automatically switches over to DC operation from the battery pack. The battery pack will then provide up to eight hours of dependable emergency communications.

Like all YAESU Amateur gear, the FT-2F comes to you with our 90-day warranty. Plus all the hardware you need to get on the air immediately — mike, connectors, DC power cord and mobile mounting bracket. The special noise-cancelling microphone contains two dynamic inserts connected out of phase to shut off external noise.

If you have ever wanted to explore two metres, the time is NOW! And the rig is the YAESU FT-2F!

## FT-2F SPECIFICATIONS

### GENERAL:

Frequency Coverage: 144 to 148 MHz.  
Number of Channels: 12 Channels (three supplied).  
Modulation: Frequency Modulation.  
Transmitter Control: Push-to-Talk.  
Power Drain: Receive 0.5 amps., transmit 2 amps.  
Power Source: DC 13.5 volts, plus or minus 10%.  
Dimensions and Weight: 6 1/2 in. w. x 2 1/2 in. h. x 10 in. d.; 4 lbs.  
Standard Accessories provided: Dynamic Microphone, Connector Plug, DC Cord—Fuse, Mobile Mount.

### TRANSMITTER:

RF Output Power: 10 Watts (high position), 1 watt (low position).  
Frequency Deviation: 15 KHz. maximum.  
Frequency Stability: Plus or minus 0.061% or less.  
Spurious Radiation: At least -60 dB. below Carrier.  
Tone Burst: Nominal 2800 Hz.

## FT-2F SPECIFICATIONS (continued)

### RECEIVER:

Receiver Circuit: Crystal-controlled Double Conversion Superhet.  
Intermediate Frequencies: 10.7 MHz. and 455 KHz.  
Sensitivity: 0.3 uV. for 20 dB. S plus N/N Ratio.  
Selectivity: Plus or minus 15 KHz. —6 dB.  
Selectivity: Plus or minus 25 KHz. —50 dB.  
Audio Output: 1 Watt.  
Speaker: 2 inch Dynamic.

## FP-2 AC POWER SUPPLY SPECIFICATIONS

Output: 13.5 volts, 2 amps.  
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